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LOADS CALIBRATIONS OF STRAIN GAGE BRIDGES ON THE DAST PROJECT AEROELASTIC RESEARCH WING (ARW-1)

FOR REFERENCE

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# LOADS CALIBRATIONS OF STRAIN GAGE BRIDGES ON THE DAST PROJECT AEROELASTIC RESEARCH WING (ARW-1)

by

#### Clinton V. Eckstrom

#### **ABSTRACT**

This paper presents details of and results from the procedure used to calibrate strain gage bridges for measurement of wing structural loads, i.e., shear (V), bending moment (M), and torque (T), for the DAST project ARW-1 wing which has an aspect ratio of 6.8, a quarter-chord line sweepback angle of 42.24°, and a taper ratio of 0.36. Results are in the form of loads equations and comparison of computed loads vs. actual loads for two simulated flight loading conditions.

#### INTRODUCTION

The first Aeroelastic Research Wing (ARW-1) undergoing flight testing as part of the Drones for Aerodynamic and Structural Testing (DAST) program is a supercritical wing of shape and planform similar to that of the F-8 supercritical wing airplane (reference 1) but of smaller size as appropriate for the BQM-34F drone aircraft. The primary purpose of this wing (ARW-1) is to evaluate an active control-flutter suppression system. The secondary purpose of the ARW-1 is to evaluate the effects of wing flexibility on aerodynamic loads measurements obtained over a range of Mach number and dynamic pressure flight test conditions. The aerodynamic loads measurements are being obtained in two forms, i.e., directly through chordwise surface pressure measurements and indirectly or in integrated form through determination of the structural loads, shear (V), bending moment (M), and torque (T). The surface pressure measurements are obtained at four spanwise stations on the right wing semi-span. The structural loads, which are derived from strain gage bridge measurements, are obtained at two spanwise stations on the right wing semi-span and at one station on the left wing semi-span.

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The purpose of this paper is to document the procedures used to obtain the equations which define the relationship between structural loadings, V, M and T, and the strain gage bridge outputs and to provide an evaluation of the accuracy of the equations by comparison of computed vs. actual loads for two simulated flight loading conditions.

#### **SYMBOLS**

Li	ith general load (V, M, or T)
M	bending moment, N-m (inlbs)
Т	torque, N-m (in1bs)
V	shear, N (1bs)
$^{eta}$ ij	coefficient of jth bridge for ith load equation, load/mV
$^{\mu}\mathbf{j}$ ,	output of jth bridge, mV
$X^M$ , $A^M$	axis system oriented perpendicular and parallel to wing 25 percent chord line with origin at vehicle centerline
r <sub>W</sub> , r <sub>W</sub>	left wing axis system perpendicular and parallel to the wing 25 percent chord line with origin at $Y_W = 1.118 \text{ m}$ (44.0 in.)
<sup>X</sup> W2, YW2	right wing axis system perpendicular and parallel to the wing 25 percent chord line with origin at $Y_W = 1.118 \text{ m}$ (44.0 in.)
x <sup>M3</sup> , x <sup>M3</sup>	right wing axis system perpendicular and parallel to the wing 25 percent chord line with origin at $Y_W = 1.880 \text{ m}$ (74.0 in.)

#### WING AND INSTRUMENTATION

#### Wing

The ARW-1 is an early type supercritical wing designed for cruise at a high transonic speed (Mach number of 0.98). The airfoil shapes are defined in reference 2, and the wing characteristics are listed in table I. The general arrangement of the BQM-34F drone aircraft with the ARW-1 wing is shown in figure 1 and a photograph of the aircraft and wing during assembly check out is shown in figure 2.

The wing structure consists of a wing center section and right and left wing panels with removable leading and trailing edges and tip section as shown in figure 3. The wing center section was machined from a thick aluminum plate in a configuration to provide a high degree of stiffness without consideration of minimum weight. The center section is located on the fuselage at the same position as the standard target drone wing and uses the same attachment bolt locations. The outboard ends of the center section are in a plane normal to the 25-percent chord line of the outer wing panels.

The primary structure of the wing panels, as shown in the photograph of figure 4, consists of a spar at the 25-percent chord line, a spar at the 60-percent chord line, upper and lower stringers at the 42.5-percent chord line, and ribs located perpendicular to the front spar (on a 12-inch spacing). A special tip rib functions as an outboard spar end fitting. The upper and lower fiberglass skins between spars are riveted in place whereas the fiberglass skins for the leading and trailing edge sections, and the tip section are held in place with removable screw fasteners. The wing panels fasten to the center section with two tension bolts at each spar.

The front and rear spars are fabricated of 17-4 PH stainless steel material whereas the stringers, ribs and outboard spar end fitting are fabricated of 7075-T6 aluminum alloy. Fiberglass was selected as the skin material and oriented to give low torsional stiffness as desired for flutter considerations. This was achieved by aligning the fiberglass filaments parallel and perpendicular to the wing front spar so that the torsional stiffness is essentially the stiffness of the binder material (matrix).

#### Vehicle Assembly

To accomplish the loads calibration of the ARW-1 wing, it was assembled on a new, spare, BQM-34F fuselage. The assembly included the wing gloves which were mounted to the fuselage. The entire assembly was inverted and placed on a special stand as shown in figure 5. The assembly was inverted for the loadings so that the inert masses (shot bags seen hanging from the wing in fig. 5) could conveniently apply forces in the proper direction.

Some negative loadings were also required and these were achieved by means of a cable-pulley arrangement.

#### Strain Gage Bridges

The wing was equipped with two identical sets of strain gage bridges, some oriented to be primarily responsive to shear loads and others to bending moment loads, at eight locations as shown in figure 6. A total of 32 strain gage bridges were installed. One set of 16 bridges consisting of one shear and bending moment strain gage bridge at each location is monitored during flight testing for loads measurement purposes. Individual gages in the second set of 16 shear and bending moment type strain gage bridges are available for backup use in case of failure of a primary bridge or for use as sensors for monitoring wing flutter. Two additional torsion-sensitive strain gage bridges were located inboard on each wing semi-span as sensors for monitoring wing flutter but they are not reported on herein.

The triangular arrangement of the bridges at the inboard station on each wing half gives special consideration to the use of axis systems oriented either parallel and perpendicular to the fuselage center line or parallel and perpendicular to the wing 25-percent chord line (along the front spar); the latter will be referred to as a swept axis system. The bridges at the midwing location on the right wing half are oriented for the swept axis system only. Initially the swept axis system was oriented parallel and perpendicular to the 42.5 percent chord line (midway between the front and rear spar) since it was considered that this would be closer to the wing elastic axis. However, the swept axis was shifted to the 25 percent chord line (along the front spar) when it was found that the torsion load data correlated much better with the strain gage bridge outputs when the 25 percent chord line axis was used as the reference. Although the bridge arrangement at the inboard stations allows use of axis systems parallel and perpendicular to the fuselage centerline, the construction of the wing and the aspect ratio and sweep of the ARW-1 wing make the swept axis system more appropriate for use in following analysis.

Tables II and III identify the various strain gage bridges by assigned number, the mounting structure, the spanwise location, and the bridge type.

Note that on the right wing bridge no's. I through 10 constitute a set and that bridges 11 through 20 are an identical set with identical bridges having a numbering difference of 10 (i.e., bridges numbered 1 and 11 are identical as are 2 and 12, etc.). On the left wing the same numbering system was used (i.e., bridges numbered 21 and 31 are identical).

All of the strain gage bridges were subjected to an input or excitation of 10 volts. It should be noted that none of the strain gage bridge circuits had provisions to zero the bridge output for the zero load condition. Therefore, it was necessary to subtract out the zero load bridge output from all of the strain gage bridge readings taken during the calibration loading process. Shunt resistors were later added to the bridge circuitry to shift or bias the zero load bridge output so that during flight testing the expected bridge output variation would not exceed the available range of the telemetry channels on the aircraft downlink data system.

The selection of which one of a pair of identical strain gage bridges was to be monitored for the initial flight loads measurements setup and which one should remain as the spare or backup was based on the ease with which the individual bridges could be biased and amplified to make the best use of the available range on the telemetry downlink channel. The selected use status for each bridge is also defined in tables II and III. Only those strain gage bridges that were to be monitored for flight loads measurement purposes are considered as being available for inclusion in the regression analysis procedure to be discussed later.

#### CALIBRATION PROCEDURE

The calibration procedure consisted of: (1) determining the electrical imbalance or output of the strain gage bridges for a large variety of wing loading conditions and (2) using a regression analysis as described in reference 3, to establish a relationship (in the form of loads equations) between the strain gage bridge outputs and the applied wing loads in terms of shear (V), bending moment (M), and torque (T). Additional wing loadings were then used to check the accuracy of the established loads equations. For the ARW-1, results from both point and multipoint loading conditions were combined and used as input data to establish the loads equations. Two

different sets of simulated flight loadings were applied and used to check the accuracy of the established loads equations.

#### Single Point Loading Conditions

Single point loads were applied individually at the locations shown in figure 7. Table IV lists the magnitudes of the applied loads and the x and y location of the point of application. The resulting differential electrical imbalance or output of each of the strain gage bridges for each of the single point loadings is listed in Table V along with the wing loading in terms of shear (V), bending moment (M), and torque (T) for the appropriate wing station. These data, along with similar data from the multipoint loadings, were used as the input to the regression analysis for determination of the loads equations.

The loads applied along the stringer located between the spars was by means of scale weights placed on a 4-in. by 4-in. square pad of aluminum with a lower surface of soft rubber so that the wing surface would not be damaged. Application of loads at all other locations was provided for by removing a screw holding the wing skin leading edge, trailing edge or tip section, and replacing it with an eye screw. With the wing in the inverted position the loads listed in Table IV were achieved by hanging either scale weights or lead shot bags from the eye screws inserted in the wing upper surface.

#### Multipoint Loading Conditions

The steps in applying loads for the multipoint loading process are listed in Table VI. Note that the loads were applied sequentially in 12 increments on each wing, with each additional load at a new location, and that the sequence was repeated three times for a total of 36 loading conditions on the up load. By following the same sequence during the down loading process an additional 33 distinct loading conditions were achieved along with three repeats of previous loading conditions. The electrical imbalance or output of each of the strain gage bridges as measured for each of the 72 steps in the process is listed in Table VII.

For the multipoint loading procedure all loads were again applied by hanging weights from eye screws on the wing upper surface. The photograph of figure 5 was taken during the multipoint loading procedure near the maximum loading condition. Equal loads were applied to or removed from both the right and left wing semi-spans at each step of the loading procedure to prevent large moments which could cause rotation of the fuselage in the support stand.

#### Simulated Flight Loading Conditions

The loadings and locations for the two simulated flight loadings are defined in tables VIII and IX and the electrical imbalance or output of each strain gage bridge is listed in table X. The first simulated flight loading represented the design loading condition analyzed for the straight and level flight at cruise condition. The second simulated flight loading represented the  $2\frac{1}{2}$ -g loading analyzed as the maximum load for stress analysis. All loads on both wing semi-spans were in the positive direction and were applied by hanging weights from eye screws. For each loading condition the entire load was applied before the strain gage bridge outputs were recorded.

#### Loads Equations

Loads equations for calculating wing loadings as a function of the output of selected strain gage bridges were determined by means of the standard regression analysis methods described in reference 3. These load equations have the form:

where  $\beta_{ij}$  is the coefficient of the jth bridge for ith load, and  $\mu_j$  is the output of the jth bridge.

The regression analysis can be performed using one or as many of the strain gage bridges as are available at each wing station. A stepwise regression analysis procedure (reference 4) was used which selects the best single strain gage bridge, then goes on to select a second bridge that, when used with the first bridge selected, gives the best combination of two bridges and continues on in the same manner to include as many bridges as are available for the location and axis system being used. The structural loads equations presented herein are for the swept axis system only. For example, for the right wing inboard station swept axis system, only strain gage bridges 13, 4, 15, and 6 were used in the regression analysis. Similarily for the left wing inboard station only strain gage bridges 23, 34, 35, and 36 were in the regression analysis.

Data from both the single-point and the multipoint loadings (tables V and VII) were combined and used as input for the regression analysis. Table XI indicates which bridges were selected for each load measurement, shear (V), bending moment (M), and torque (T), and presents the associated load coefficients  $(\beta_{\mbox{\scriptsize i},\mbox{\scriptsize i}})$  and probable errors along with the standard error of estimate for the equation and the multiple correlation coefficient which is an indication of how well the calibration data fit the linear regression equation selected. In all cases, except one, the multiple correlation coefficient is better than 0.9990. (A value of zero being no fit and a value of 1.0 being a perfect fit.) The one exception is for the torque equation for the right wing midwing station where the multiple correlation coefficient is 0.99754. Figures 8 through 16 provide a visual idea of how well the selected loads equations correlate with the data from which they are 'derived. These figures present load as calculated using the selected loads equations as a function of applied load for both single point and multi-point loadings. For a perfect correlation all the data would fall on a straight line with a one to one relationship between applied load and computed load.

The selected load equations were also used to estimate the loads applied during the two simulated flight loadings, table X. Results are presented in

table XII. For all shear and bending moment loads the selected load equations predicted the loads within ±4 percent of the actual applied load. For the torsion moment loads the selected loads equations were less accurate. For the load simulating the straight and level design point flight condition, the equations underpredicted the torsion load by 4 to 8 percent. For the load simulating a 2.5 g maneuver flight condition, the equations overpredicted the torsion load 3 to 5 percent at the inboard stations and by 26 percent at the right wing midwing station. The results are considered satisfactory except for the torque load estimate for the right wing midwing station.

#### CONCLUDING REMARKS

The ARW-1 Aeroelastic Research Wing consists of conventional spar, stringer, rib and skin construction. Strain gage bridges sensitive to shear and bending moment loads were installed for load measurement purposes at two spanwise locations on the right wing half and at one location on the left wing half. Results from both the single point and multipoint loadings were combined for use as input to the stepwise regression analysis used to derive loads equations for each load type (V, M, and T) at each wing station. Comparison of loads predicted using the derived loads equations with actual applied loads for the two simulated flight loading conditions indicated excellent results for shear and bending moment loads (within ±4 percent). At the right and left inboard wing stations, the predicted torsion loads are good (within ±6 percent). The predicted torsion loads at the right wing midwing station were less accurate than desired (error ranging from 8 to 26 percent).

#### REFERENCES

- 1. Anon.: Supercritical Wing Technology A Progress Report on Flight Evaluations. NASA SP-301, 1972.
- 2. Byrdsong, Thomas A.; and Hallissy, James B.: Longitudinal and Lateral Static Stability and Control Characteristics of a 1/6-Scale Model of a Remotely Piloted Research Vehicle With a Supercritical Wing. NASA TP-1360, 1979.
- 3. Skopinski, T. H.; Aiken, William S., Jr.; and Huston, Wilber B.: Calibration of Strain-Gage Installations in Aircraft Structures for the Measurement of Flight Loads. NACA Rep. 1178, 1954. (Supersedes NACA TN 2993)
- 4. Furnival, G. M.; and Wilson, R. W.: Regressions by Leaps and Bounds.

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TABLE I.- WING CHARACTERISTICS

Aspect ratio	6.8	
Taper ratio	0.36	
Sweepback angle at ¼ chord line, deg.	42.24	
Reference area, m <sup>2</sup> (ft. <sup>2</sup> )	2.78	(30.0)
Thickness at root, percent chord	11.0	, ,
Thickness at tip, percent chord	7.0	
Span, m (in.)	4.343	(171.0)
Tip chord length, m (in.)	0.343	(13.51)
Root chord length, m (in.)	0.940	(36.99)
Mean aerodynamic chord (MAC) length, m (in.)	0.687	(27.06)

TABLE II.- IDENTIFICATION OF STRAIN-GAGE BRIDGES -RIGHT WING

Bridge No.	Structure	Y	I	Bridge Type	Use
Í	F.S.	m 0.927	(in.) (36.5)	V	Backup
Ž	F.S.	0.927	(36.5)	М	Loads
3	F.S.	1.118	(44.0)	V	Backup
4	F.S.	1.118	(44.0)	М	Loads
5	R.S	1.118	(44.0)	V	Backup
6	R.S.	1.118	(44.0)	М	Loads
7	F.S.	1.880	(74.0)	V	Loads
8	F.S.	1.880	(74.0)	M	Backup
9	R.S.	1.880	(74.0)	V	Loads
10	R.S.	1.880	(74.0)	M	Loads
11	F.S.	0.927	(36.5)	٧	Loads
12	F.S.	0.927	(36.5)	M	Backup
13	F.S.	1.118	(44.0)	γ.	Loads
14	F.S.	1.118	(44.0)	M	Backup
15	R.S.	1.118	(44.0)	V	Loads
16	R.S.	1.118	(44.0)	M	Backup
17	F.S.	1.880	(74.0)	V	Flutter
18	F.S.	1.880	(74.0)	М	Loads
19	R.S.	1.880	(74.0)	٧	Backup
20	R.S.	1.880	(74.0)	M	Backup

F.S. = front spar, R.S. = rear spar, V = shear, M = bending moment.

TABLE III.- IDENTIFICATION OF STRAIN-GAGE BRIDGES - LEFT WING

	~		•	****	
Bridge No.	Structure	m Y	d (in.)	Bridge Type	Use
		(1)	(111.)	•	
21	F.S.	0.927	(36.5)	٧	Backup
22	F.S.	0.927	(36.5)	M	Backup
23	F.S.	1.118	(44.0)	V.	Loads
24	F.S.	1.118	(44.0)	М	Backup
25	R.S.	1.118	(44.0)	V	Backup
26	R.S.	1.118	(44.0)	M	Backup
31	F.S.	0.927	(36.5)	V	Loads
32	F.S.	0.927	(36.5)	M	Loads
33	F.S.	1.118	(44.0)	V	Flutter
34	F.S.	1.118	(44.0)	M	Loads
35	R.S.	1.118	(44.0)	٧	Loads
36	R.S.	1.118	(44.0)	М	Loads

F.S. = front spar, R.S. = rear spar, V = shear, M = bending moment.

TABLE IV. - SINGLE POINT APPLIED LOADS AND LOCATIONS

Part A. - Left Wing, Inboard Station

į.						
Location No.	Appli	ed Load		Location	Coordinates	
(See Fig. 7)	N	(1bs)	·	$Y_{W,1}$	$x_{W_{.1}}$	
			m	(in.)	m	(in.)
1	890	(200)	0.058	(2.30)	-0.012	(-0.47)
2	890	(200)	0.066	(2.60)	0.095	(3.75)
3	890	(200)	0.058	(2.29)	0.203	(8.00)
4	712	(160)	0.363	(14.30)	-0.012	(-0.47)
5	712	(160)	0.371	(14.60)	0.087	(3.44)
6	712	(160)	0.362	(14.26)	0.185	(7.30)
7	712	(160)	0.670	(26.36)	-0.012	(-0.49)
8	712	(160)	0.675	(26.56)	0.079	(3.10)
9	712	(160)	0.667	(26.26)	0.168	(6.60)
10	667	(150)	0.975	(38.37)	-0.013	(-0.50)
11	445	(100)	0.979	(38.56)	0.071	( 2.80)
12	667	(150)	0.972	(38.28)	0.151	(5.96)
13	534	(120)	1.279	(50.34)	-0.012	(-0.47)
14	222	(50)	1.285	(50.58)	0.061	( 2.42)
15	534	(120)	1.278	(50.32)	0.134	(5.28)
16	356	(80)	1.578	(62.13)	-0.011	(-0.45)
17	222	(50)	1.667	(65.63)	0.048	(1.90)
18	356	(80)	1.723	(67.83)	0.110	( 4.35)

TABLE IV. - Continued

Part B. - Right Wing, Inboard Station

Location No.		ied Load		Location Co	ordinates	
(See Fig. 7)	· N	(1bs)		Y <sub>W2</sub> (in)	X <sub>V</sub>	la '
			m	<sup>2</sup> (in)	m	(in)
1	222	(50)	0.063	(2.48)	-0.089	(-3.52)
2	890	(200)	0.054	(2.14)	-0.013	(-0.51)
3	890	(200)	0.066	(2.60)	0.095	(3.75)
4	890	(200)	0.056	(2.21)	0.202	(7.95)
5	267	(60)	0.066	(2.60)	0.330	(12.98)
6	890	(200)	0.217	(8.13)	-0.013	(-0.50)
7	890	(200)	0.208	(8.19)	0.194	(7.62)
8	222	(50)	0.369	(14.51)	-0.083	(-3.25)
9	712	(160)	0.362	(14.26)	-0.012	(-0.48)
10	667	(150)	0.371	(14.60)	0.087	( 3.44)
11	712	(160)	0.362	(14.26)	0.185	(7.30)
12	267	(60)	0.368	(14.50)	0.273	(10.75)
13	667	(150)	0.511	(20.12)	-0.013	(-0.50)
14	667	(150)	0.515	(20.26)	0.177	(6.98)
15	133	(130)	0.674	(26.55)	-0.074	(-2.90)
16	667	(150)	0.665	(26.20)	-0.012	(-0.49)
17	667	(150)	0.675	(26.56)	0.079	(3.10)
: 18	667	(150)	0.669	(26.32)	0.168	(6.60)

TABLE IV. - Continued

Part B. - Concluded

Location No.	App1	ied Load			n Coordinates	
(See Fig. 7)	N	(1bs)	Y	W <sub>2</sub>	X	<sup>N</sup> 2
			m	(in.)	m	(in)
19	133	(30)	0.673	(26.50)	0.241	(9.48)
20	667	(150)	0.818	(32.21)	-0.013	(-0.50)
21	667	(150)	0.820	(32.27)	0.160	(6.30)
22	200	( 45)	0.979	(38.56)	-0.053	(-2.10)
23	667	(150)	0.971	(38.22)	-0.013	(-0.50)
24	400	(90)	0.979	(38.56)	0.071	( 2.80)
25	667	(150)	0.971	(38.24)	0.151	(5.96)
26	200	( 45)	0.980	(38.60)	0.206	(8.10)
27	534	(120)	1.124	(44.25)	-0.012	(-0.49)
28	534	(120)	1.127	(44.36)	0.143	(5.63)
29	200	( 45)	1.287	(50.68)	-0.048	(-1.88)
30	534	(120)	1.275	(50.19)	-0.012	(-0.49)
31	267	(60)	1.285	(50.58)	0.061	( 2.42)
32	534	(120)	1.280	(50.38)	0.134	(5.28)
34	400 <sup>-</sup>	(90)	1.444	(56.86)	-0.011	(-0.45)
35	400	(90)	1.441	(56.75)	0.127	(5.00)
36	200	( 45)	1.547	(60.91)	-0.041	(-1.63)
37	400	(90)	1.574	(61.96)	-0.011	(-0.45)
38	267	(60)	1.666	(65.58)	0.050	(1.95)
39	400	(90)	1.720	(67.70)	0.112	( 4.40)
40.	200	(45)	1.745	(68.72)	0.141	(5.55)

TABLE IV. - Concluded

Part C. - Right Wing, Midwing Station

Location No.	App	lied Load	Location Coordinates			
(See Fig. 7)	N	(1bs)	,	A <sup>M3</sup>	$x_{l}$	<sup>1</sup> 3
			m	(in)	m	(in)
20	667	(150)	0.056	(2.21)	-0.013	(-0.50)
21	667	(150)	0.058	(2.27)	0.160	(6.30)
22	200	( 45)	0.217	(8.56)	-0.053	(-2.10)
23	667	(150)	0.209	(8.22)	-0.013	(-0.50)
24	400	(90)	0.217	(8.56)	0.071	( 2.80)
25	667	(150)	0.209	(8.24)	0.151	(5.96)
26	200	( 45)	0.218	(8.60)	0.206	(8.10)
27	534	(120)	0.362	(14.25)	-0.012	(-0.49)
28	534	(120)	0.365	(14.36)	0.143	(5.63)
29	200	(45)	0.525	(20.68)	-0.048	(-1.88)
30	534	(120)	0.513	(20.19)	-0.012	(-0.49)
31	267	(60)	0.523	(20.58)	-0.061	( 2.42)
32	534	(120)	0.518	(20.38)	0.134	(5.28)
34	400	(90)	0.682	(26.86)	-0.011	(-0.45)
35	400	(90)	0.679	(26.75)	0.127	(5.00)
∃36	200	( 45)	0.785	(30.91)	-0.041	(-1.63)
37	400	(90)	0.812	(31.96)	-0.011	(-0.45)
38	267	(60)	0.904	(35.58)	0.050	(1.95)
39	400	(90)	0.958	(37.70)	0.112	( 4.40)
40	200	( 45)	0.983	(38.72)	0.141	(5.55)

TABLE V.- WING EDADINGS AND STRAIN-GAGE BRIDGE DUTPHTS FOR SINGLE-POINT APPLIED LOADS ...

WING LOADINGS

SHEAR, LBS	MOMENT, IN-LBS	TORQUE, IN-LPS	MU 21	MU 22	MU 23	MU 24	MU 25	MU 26	MU 31	MU 32	MU 33	MU 34	4U 35	MU 36
200.00	460.00	-94.00	•651	.810	•778	038	•126	•373	•655	.843	•796	051	•120	•369
200.00	520.00	750.00	•392	•699	•440	.244	•492	.285	•392	.719	.425	• 365	• 474	.388
200.00	458.00	1600.00	.108	•581	.145	• 330	•936	019	•110	.591	•138	.315	922	•007
160.00	2288.00	<b>-</b> 75•20	• 423	1.452	•510	1.013	•138	.816	.429	1.485	•498	1.072	•133	.848
160.00	2336.00	550.40	• 253	1.272	•308	•929	•407	•951	.255	1.306	.295	961	.396	1.002
160.00	2281.60	1168.00	•126	1.087	•159	•837	.613	1.026	.130	1.114	151	.866	.594	1.113
160.00	4217.60	-78.40	.377	2.227	•422	1.861	•117	1.507	•387	2.260	•415	1.945	.188	1.581
160.00	4249.60	496.00	.249	2.036	•272	1.752	•327	1.687	•257	2.061	•267	1.833	•324	1.784
160.CO	4201.60	1056.00	•127	1.824	.137	1.612	•527	1.810	•133	1.670	.132	1.685	•513	1.934
150.00	5755.50	-75.00	.314	2.718	.319	2.446	•092	2.070	•326	2.790	•316	2.553	•094	2.175
100.00	3356.00	280.00	•137	1.720	•131	1.594	•176	1.500	-140	1.759	•131	1.667	.175	1.585
150.00	5742.00	894.00	.110	2.388	.089	2.238	• 420	2.334	•119	2.442	.069	2.343	•411	2.472
120.00	5040.80	-56.40	.223	2.688	•202	2.524	•054	2.190	•234	2.749	•204	2.635	•060	2.303
50.00	2529.00	121.60	• 060	1.088	•047	1.047	.074	•976	•064	1.111	•047	1.095	•076	1.031
120.00	6038.40	633.60	·C78	2.467	.03€	2.387	-281	2.375	•288	2.531	.041	2.500	•281	2.512
80.00	4970.40	-36.00	•126	2.126	•097	2.057	•021	1.008	•138	2.177	•101			
50.00	3281.50	95.00	•051	1.378	.027	1.366	•050	1.066	•056	1.408	•101	2.147	•026	1.900
80.00	5426.40	348.00	.038	2.160	.012	2.161	•144	2.080	•046	2.209	•005	1.428 2.226	•055 •146	1.322 2.190

#### TABLE V.- CONTINUED

#### (B) RIGHT WING, INBOARD STATION

#### WING LOADINGS

SHEAR.	MOMENT.	TORQUE												
LBS	IN-LBS	IN-LES	MU 1	MU 2	MU 3	MU 4	MU 5	MU 6	MU 11	MU 12	MU 13	MU 14	MU 15	MU 16
50.00	124.00	-176.00	•176	•227	• 206	•016	•011	.101	•182	•229	•194	•011	006	.078
200.00	428.00	-102.00	•673	•₹12	•791	048	•119	•378	<b>.</b> 674	• 524	•777	07€	•116	•338
200.00	520.00	750.00	•388	•665	•385	• 254	•550	• 289	•363	•673	•364	•301	•521	•376
200.00	442.00	1590.CO	• 096	•588	•124	•333	•992	• 002	•094	•588	•110	•309	•991	•02C
60.00	156.00	778.80	<b></b> 050	•138	049	• 094	• 405	•049	051	.139	048	•065	• 392	.066
200.00	1626.00	-100.00	•615	1.349	•724	•662	•147	•667	•617	1.368	•692	•691	•142	•632
200.00	1638.00	1524.00	•136	•927	•156	•638	.878	•778	•133	•942	•142	.637	.847	.823
50.00	725.50	-162.50	•172	•482	•191	• 322	009	• 241	•175	• 495	•182	• 333	006	• 229
160.00	2281.60	−76∙ ⊧0	• 454	1.467	•501	1.012	•134	•838	•460	1.489	•482	1.042	•132	.804
150.00	2190.00	516.00	• 253	1.192	•278	<ul><li>866</li></ul>	•379	•938	.254	1.202	•264	.878	.368	• 929
160.00	2281.60	1169.00	•126	1.C78	•133	<ul><li>824</li></ul>	•631	1.128	•127	1.091	•122	.826	•608	1.154
60.00	970.00	645.00	006	•364	008	•300	•312	• 443	007	• 374	012	•307	.303	.447
150.00	3018.00	-75.00	• 405	1.712	• 422	1.330	•118	1.118	• 409	1.731	•410	1.361	•118	1.055
150.00	3039.00	1047.60	•129	1.340	•121	1.105	•538	1.453	•130	1.356	•111	1.130	•522	1.469
30.00	796.50	-87.00	• 090	•420	•090	•356	•003	• 268	•092	•421	•089	•371	•001	•261
150.00	3930.00	<del>-</del> 73•50	•389	2.068	•362	1.710	•112	1.438	•394	2.086	.371	1.742	.113	1.410
150.00	3984.00	465.00	• 243	1.860	•223	1.531	•325	1.665	•243	1.879	•213	1.622	•318	1.659
150.00	3948.00	990.00	•134	1.684	•108	1.467	•496	1.828	•135	1.706	.101	1.504	.485	1.836
30.00	795.00	284.40	•006	•311	.001	• 274	•123	• 377	•006	•317	002	• 266	.120	•379
150.00	4831.50	<del>-</del> 75.00	•368	2.348	•334	2.029	•102	1.771	•371	2.371	•327	2.070	•103	1.740
150.00	4840.50	945.00	•136	2.006	•091	1.800	.445	2.130	•137	2.030	.084	1.846	.436	2.129
45.00	1735.20	-94.50	•117	.801	.102	•733	•004	•615	•118	.809	.100	•747	.007	.605
150.00	5733.00	<del>-</del> 75.00	•358	2.691	•361	2.386	•087	2.124	•364	2.717	.297	2.310	•090	2.091
90.00	3470.40	252.OC	•139	1.525	.101	1.394	•164	1.417	.141	1.539	.100	1.425	.163	1.407
150.00	5736.00	894.00	.138	2.360	.071	2.170	•413	2.474	•139	2.384	.067	2.221	.405	2.469
45.00	1737.00	364.50	•011	•674	004	•638	•152	•769	.015	.654	005	•654	.150	•766
120.00	5310.00	-58.80	<b>-</b> 269	2.379	.208	2.175	.061	1.977	.273	2.401	.206	2.218	•065	1.950
120.00	5323.20	675.60	•102	2.146	•035	2.028	•304	2.236	•104	2.164	.035	2.077	• 301	2.226
45.00	2280.60	-84.60	•105	•983	.078	•934	002	.821	•108	•991	.079	952	.001	.809
120.00	6022.80	-58•€C	• 261	2.657	•183	2.462	•049	2.267	.265	2.681	.185	2.509	•056	2.236
60.00	3034.80	145.20	•084	1.278	•043	1.223	•090	1.222	•086	1.288	.044	1.250	• 090	2.212
120.00	6045.60	633.60	•106	2.424	•020	2.320	•276	2.503	.108	2.451	.020	2.374	.276	2.491
90.00	5117.40	-40.50	.184	2.181	•111	2.072	•027	1.923	.188	2.200	•114	2.111	•034	1.898
90.00	5107.00	450.CO	•073	2.019	003	1.964	.189	2.081	•075	2.039	000	2.011	•190	2.067
45.00	2740.95	-73.35	•097	1.144	.058	1.110	•008	1.003	•099	1.152	.059	1.130	•002	988
90.00	5576.40	-40.50	.179	2.352	.095	2.255	.019	2.108	192	2.372	.099	2.296	•026	2.078
60.00	3934.80	117.00	·C85	1.615	•023	1.563	.061	1.544	•088	1.628	•025	1.594	•066	1.528
90.00	6093.00	396.00	.073	2.453	027	2.364	.156	2.455	•050	1.618	014	1.610	•105	1.624
45.00		249.75	•020	1.170	032	1.176	•091	1.238	•023	1.182	027	1.202	•093	1.230
		- · · • · •					40,1		4063	10102	- 4021	TOCAC	• 0 7 3	10520

TAPLE V.- CONCLUDED

#### (C) RIGHT WING, MIDWING STATION

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	UTNC	1 mai	D T N C

SHEAR, LBS	MOMENT, IN-LPS	TORQUE, IN-LBS	MU 7	MU 8	MU 9	MU 10	MU 17	MU 18	MU 19	MU 20
150.00	331.50	-75.0C	•924	039	•117	4.70	044	107	107	
150.00	340.50	945.00				• 479	•968	107	•107	•419
			•126	•500	1.116	333	•116	• 453	1.164	<b></b> 413
45.00	385.20	-94.50	• 266	•264	•025	• 293	<ul><li>253</li></ul>	• 257	•021	• 274
150.00	1233.00	<b>-75.</b> 00	• E79	•679	•174	•910	•832	•868	•156	.859
90.00	770.40	252.00	•304	•590	•371	•517	.285	•582	• 352	• 486
150.00	1236.00	894.00	•183	•960	•921	•730	.166	.933	.887	•696
45.00	387.00	364.50	.013	•304	•312	• 206	•009	.292	•303	.168
120.00	1710.00	-58.80	•591	1.327	•170	1.138	•554	1.323	.139	1.089
120.00	1723.20	675.60	.181	1.220	.621	1.198	•162	1.208	591	1.143
45.00	930.60	-84.60	•215	•717	•034	•608	•201	•714	•027	•583
120.00	2422.80	-58.60	.513	1.886	•174	1.605	•479	1.880	•153	1.535
60.00	1234.80	145.20	.165	•923	192	.866	•154			
120.00	2445.60	633.60	•185					•920	•179	•826
_				1.726	•539	1.734	•162	1.534	•509	1.661
90.00	2417.40	-40.50	•330	1.844	.122	1.608	• 305	1.841	•101	1.542
90.00	2407.50	450.00	•122	1.714	•359	1.686	•105	1.713	•333	1.616
45.00	1390.95	<b>-73∙3</b> 5	•171	1.057	•031	.919	•159	1.064	•018	.881
90.00	2876.40	-40.50	• 295	2.179	•107	1.930	.271	2.177	.085	1.085
60.00	2134.80	117.00	•131	1.551	•141	1.439	•115	1.550	.122	1.375
90.00	3393.00	396.00	.087	2.454	.291	1.938	.045	1.638	1.174	1.503
45.00	1742.40	249.75	.019	1.238	•166	1.203	•009	1.239	•150	1.149

TABLE VI. - MULTIPOINT APPLIED LOADS, LOCATIONS AND APPLICATION SEQUENCE.

		AP	PLIED LOAD	n		- · · · - · ·			FEICHIIO	א סבעטבאנ	JE.		
LOADING		CREMENT:	S TOTA	AL .	LEFT WING	, INBOARD	RIG	LOCATIO HT WING,	IN TÙROARD		DIA	NIT 11	_
STEP	N (E)	a <mark>ch Win</mark> g 1bs	y) (Each	Wing) (lbs	$\sim Y_{\rm LJ}$	m XW](in)		Y <sub>W2(in)</sub>	XI	√2 (in)	K16	HT WING, MIDW	ING
1							m	"2(in.)	· m	<sup>12</sup> (in.)	m 'W	3(in.) m	<sup>3</sup> (in)
2	111,21	25	111.2	25	1.723 67.83		1.720	67.70	0.112	4.40	0.958	37.70 0.11	
	111.21	25	222.4	50	1.578 62.13	-0.011 -0.45	1.574	61.96	-0.011	-0.45	0.812	31.96 -0.01	
3	111.21	25	333.6	75	1.278 50.32	0.134 5.28	1.280	50.38	0.134	5.28	0.518	20.38 0.13	
4	111.21	25	444.8	100	1.279 50.34	-0.012 -0.47	1.275	50.19	-0.012	-0.49	0.513	20.19 -0.01	
5	111.21	25	556.0	125	0.972 38.28	0.151 5.96	0.971	38.24	0.151	5.96	0.209		
6	111.21	25	667.2	150	0.975 38.37			38.22	-0.013	-0.50	0.209	8.24 0.15	
7	222.41	50	889.6	200	0.667 26.26	0.168 6.60	0.669	26.32	0.168	6.60	0.203	8.22 -0.013	3 -0.50
8	222.41	50	11112.1	250	0.670 26.36	-0.012 -0.49	0.665	26.20	-0.012	-0.49			
9	222.41	50	1334.5	300	0.362 14.26	0.185 7.30	0.362	14.26	0.185	7.30			
10	222.41	50	1556.9	350	0.363 14.30	-0.012 -0.47	0.362	14.26	-0.012	-0.48			
11	222.41	50	1779.3	400	0.058 2.29	0.203 8.00	0.056	2.21	0.202	7.95			
12	222.41	50	2001.7	450	0.058 2.30			2.14	-0.013				
13 to 36		*	6005.1	1350				2.1	-0.013	-0.51			
37	-111.21	-25	5893.9	1325	1.723 67.83	0.110 4.35	1.720	67.70	0.112	4.40	0.050		
38	-111.21	-25	5782.7	1300	1.578 62.13	0.044	1.574	61.96		4.40	0.958	37.70 0.112	
39	-111.21	-25	5671.5	1275	1.278 50.32	0.134 5.28		50.38	-0.011	-0.45	0.812	31.96 -0.011	
40	-111.21	-25	5560.3	1250	1.279 50.34	-0.012 -0.47		50.19	0.134	5.28	0.518	20.38: 0.134	
41	-111.21	-25	5449.1	1225	0.972 38.28	0.151 5.96			-0.012	-0.49	0.513	20.19 -0.012	
42	-111.21	-25	5337.9		0.975 38.37	-0.013 -0.50		38.24	0.151	5.96	0.209	8.24 0.151	
43	-222.41	-50	5115.5		0.667 26.26	0.168 6.60		38.22	-0.013	-0.50	0.209	8.22 -0.013	<b>-</b> 0.50
44	-222.41	-50	4893.0		0.670 26.36			26.32	0.168	6.60			
45	-222.41	-50	4670.5		0.362 14.26	0.185 7.30	0.665	26.20	-0.012	-0.49			
46	-222.41	-50	4448.2					14.26	0.185	7.30			
47	- 222.41		4225.8		0.058 2.29		0.362	14.26	-0.012	-0.48			
48	- 222.41		4003.4		_		0.056	2.21	0.202	7.95			
49 to 72		+	0	0	2.30	-0.012 -0.47	0.054	2.14	-0.013	-0.51			
				•									

 $<sup>\</sup>star$  Repeat steps 1 through 12 two more times.

<sup>+</sup> Repeat steps 37 through 48 two more times.

#### (A) LEFT WING, INBOARD STATION

#### WING LOADINGS

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SHEAP,	MOMENT	TORQUE												
LBS	IN-LAS	IN-LAS	MU 21	MU 22	MU 23	MU 24	MU 25	411 26	MU 31	MU 32	MU 33	MU 34	MU 35	MU 36
									.0 31	110 32	10 33	110 34	~O 35	~U 3E
25.00	1695.50	108.75	• 609	<b>*</b> 684	004	.695	•044	•663	•012	• 701	003	•727	•046	• 700
50.00	3248.75	97.50	•047	1.363	•028	1.358	•052	1.250	.055	1.391	.031	1.419	• 055	1.318
75,00	4506.75	229.50	•066	1.900	.037	1.872	•113	1.765	.074	1.941	.041	1.957	•115	1.510
100.00	5765.25	217.75	•115	2.493	•084	2.414	•125	2.251	•127	2.556	066	2.524	.128	2.378
125.00	5722.25	366.75	•136	2.925	•103	2.801	.194	2.659	.147	2.997	.105	2.931	196	2.811
150.00	7691.50	354.25	•193	3.423	•162	3.219	•208	3.029	-207	3.510	•164	3.369	-210	3.200
200.00	8994.50	684.25	•241	4.060	•213	3.736	•367	3.619	•256	4.164	.214	3.910	• 367	3.635
	10307.50	659.75	• 362	4.793	.354	4.316	.4C5	4.109	•379	4.925	.350	4.524	• 402	4.350
	11020.50	1024.75	•411	5.198	•41¢	4.596	•593	4.449	428	5.346	•406	4.811	• 587	4.722
	11735.50	1001.25	•548	5.691	•57s	4.920	.635	4.719	•565	5.859	•568	5.154	627	5.001
	11850.00	1401.25	•580	5.885	•619	5.007	.867	4.714	598	6.031	•607	5.246	857	5.001
	11965.00	1377.75	•744	6.085	•820	5.023	•901	4.º12	•762	6.27.	.510	5.231	.888	5.099
	13660.50	1486.50	• 776	6.911	• £ 3 €	5.711	.940	5.516	.793	7.146	.627	5.976	•930	5.847
	15213.75	1475.25	• €15	7.603	•875	6.372	•946	5.103	•836	7.860	.865	6.663	•938	6.463
	16471.75	1607.25	• £35	ۥ175	.892	6.889	1.005	6.618	957	6.451	.862	7.205	995	7.006
	17730.25	1595.50	• ₹86	00843	•945	7.433	1.015	7.105	.911	9.101	935	7.775	1.007	7.513
	18687.25	1744.50	•¢10	9.252	•968	7.825	1.085	7.511	934	9.566	957	8.185	1.078	7.944
	19646.50	1732.00	• 969	9.764	1.031	8.247	1.100	7.884	•994	10.099	1.020	6.629	1.093	8 • 334
	20959.50	2062 <b>.</b> 00	1.016	10.426	1.067	6.774	1.264	8.467	1.042	10.763	1.074	9.178	1.256	8.951
	22272.50	2037.50	1.139	11.193	1.233	9.362	1.305	8.970	1.170	11.565	1.217	9.799	1.294	9.476
	22985.50	2402.50	1.186	11.002	1.290	9.647	1.496	9.307	1.218	11.984	1.272	13.091	1.481	9.839
	23700.50	2379.00	1.330	12.124	1.463	9.974	1.541	9.592	1.351	12.520	1.440	10.441	1.523	10.132
	23915.00	2773.00	1.365	12.297	1.505	10.066	1.776	9.594	1.396	12.697	1.479	10.531	1.757	10.135
	23930.00	2755.50	1.528	12.525	1.706	10.061	1.612	9.695	1.560	12.935	1.600	10.522	1.791	10.237
	25625.50	2564.25	1.551	13.308	1.719	10.768	1.859	10.395	1.586	13.750	1.694	11.265	1.841	10.257
	27178.75	2853.00	1.608	14.095	1.772	11.448	1.568	11.020	1.644	14.545	1.746	11.982	1.854	11.613
	23436.75	2905.00	1.626	14.651	1.787	11.969	1.934	11.545	1.564	15.127	1.761	12.531	1.919	12.164
1000.00		2973.25	1.6P1	15.289	1.644	12.524	1.947	12.041	1.722	15.779	1.817	13.119	1.934	12.680
1025.00		3122.25	1.700	15.721	1.662	12.913	2.021	12.451	1.742	16.226	1.036	13.527	2.007	13.108
1050.00		3109.75	1.772	16.247	1.932	13.367	2.073	12.920	1.817	16.758	1.905	14.026	2.058	13.631
1100.00		3439.75	1.821	16.900	1.987	13.894	2.245	13.514	1.966	17.430	1.959	14.585	2.228	14.262
1150.00		3415.25	1.947	17.654	2.136	14.500	2.292	14.037	1.998	18.200	2.107	15.236	2.273	14.806
1200.00		3790.25	2.001	16.065	2.198	14.799	2.489	14.394	2.049	18.622	2.166	15.552	2.464	15.189
1250.00		3756.75	2.136	18.566	2.365	15.129	2.540	14.680	2.139	19.137	2.330	15.908	2.513	15.488
1300.00		4156.75	2.173	14.741	2.410	15.225	2.774	14.676	2.225	19.316	2.370	16.000	2.745	15.486
1350.00	35895.00	4133.25	2.351	19.028	2.617	15.232	2.826	14.861	2.403	19.617	2.580	16.065	2.796	15.667
		-				· <del>-</del>			- 4 , 0 3	1 / U U I	2000	10.007	7 6 1 70	T3 ● CC /

#### TABLE VII. - CONTINUED

#### (A) CONCLUDED

#### WING LOADINGS

SHEAR,	MOMENT,	TOPQUE												
LBS	IN-LBS	IN-LES	MU 21	MU 22	MU 23	MU 24	MU 25	MII 26	MU 31	MU 32	Ml: 33	MU 34	MU 35	MU 36
1325.00	34199.50	4024.50	2.352	18.378	2.624	14.597	2.782	14.211	2.403	18.956	2.584	15.352	2.752	14.077
1300.00	32646.25	4035.75	2.320	17.715	2.591	13.941	2.773	13.629	2.366	18.287	2.551	14.665	2.740	14.363
1275.00	31388.25	3903.75	2.308	17.197	2.580	13.439	2.712	13.123	2.350	17.761	2.539	14.137	2.681	13.824
1250.00	30129.75	3915.50	2.263	16.629	2.536	12.906	2.700	12.653	2.306	17.160	2.494	13.560	2.667	13.325
1225.00	29172.75	3766.50	2.243	16.202	2.515	12.526	2.628	12.247	2.285	16.745	2.475	13.162	2.597	12.896
1200.00	28213.50	3779.00	2.193	15.734	2.458	12.114	2.611	11.889	2.232	16.264	2.419	12.752	2.580	12.514
1150.00	26900.50	3449.00	2.153	15.141	2.410	11.610	2.447	11.309	2.190	15.655	2.372	12.225	2.420	11.890
1100.00	25587.50	3473.50	2.037	14.423	2.273	11.036	2.407	10.820	2.072	14.923	2.237	11.622	2.380	11.370
1050.00	24974.50	3108.50	1.996	14.056	2.219	10.767	2.213	10.482	2.030	14.545	2.164	11.366	2.194	10.997
	24159.50	3132.00	1.864	13.575	2.055	10.450	2.167	10.213	1.895	14.047	2.025	11.007	2.149	10.717
	24045.00	2732.00	1.633	13.416	2.013	10.366	1.935	10.214	1.864	13.887	1.967	10.924	1.919	10.709
900.00	23730.00	2755.50	1.671	13.202	1.812	10.373	1.901	10.117	1.702	13.661	1.786	10.935	1.887	10.612
875.00	22234.50	2646.75	1.654	12.457	1.803	9.630	1.654	9.420	1.683	12.890	1.776	10.209	1.839	9.865
	20681.25	2658.00	1.615	11.749	1.766	9.024	1.848	8.817	1.641	12.157	1.737	9.523	1.831	9.227
	19423.25	2526.CC	1.598	11.191	1.749	8.514	1.788	8.292	1.624	11.582	1.721	8.964	1.770	8.664
	18164.75	2537.75	1.549	10.585	1.697	7.974	1.775	7.800	1.574	10.951	1.669	6.424	1.758	8.143
	17207.75	2388.75	1.530	10.150	1.676	7.589	1.705	7.384	1.553	10.500	1.650	3.022	1.687	7.699
	16248.50	2401.25	1.475	9.658	1.614	7.175	1.690	7.012	1.498	9.986	1.587	7.584	1.671	7.306
_	14935.50	2071.25	1.431	9.030	1.562	6.659	1.525	6.413	1.452	9.341	1.537	7.045	1.509	6.664
	13622.50	2095.75	1.312	₺•297	1.419	6.079	1.485	5.916	1.330	8.574	1.397	6.437	1.471	6.139
	12909.50	1730.75	1.267	7.915	1.365	5.806	1.295	5.579	1.287	8.185	1.345	6.153	1.284	5.767
	12194.50	1754.25	1.132	7.418	1.195	5.499	1.251	5.305	1.149	7.663	1.181	5.618	1.242	5.517
_	12080.00	1354.25	1.099	7.252	1.154	5.400	1.018	5.304	1.116	7.497	1.142	5.732	1.011	5 • 475
	11965.00	1377.75	• 933	7.013	•948	5.403	•985	5.197	•949	7.245	•938	5.735	•980	5.369
	10269.50	1269.00	•915	6.267	•942	4.702	•937	4.495	•930	6.468	•929	5.000	•931	4.621
400.00	8716.25	1280.25	•F71	5.522	.897	4.038	•931	3.884	•893	5.698	.654	4.364	•922	3.579
375.CO	745P.25	1148.25	• £ 49	4.948	•882	3.543	<b>.</b> 870	3.358	•961	5.107	•867	3.765	.862	3.417
350.00	6199.75	1160.00	• 795	4.316	•62€	2.979	•858	2.862	•806	4.455	•814	3.192	. 8 4P	2.899
325.00	5242.75	1011.00	•771	3.865	• 605	2 • 588	•7€6	2.446	•780	3.991	•793	2.761	•777	2.458
300.00	4283.50	1023.50	•711	3.355	•743	2.170	•770	2.072	•720	3.462	•731	2.339	•760	2.067
250.00	2970.50	693.50	•653	2.691	•689	1.646	•606	1.484	•663	2.777	•676	1.769	• 599	1.441
200.00	1657.50	718.00	•515	1.911	•542	1.054	•563	•971	•521	1.966	•535	1.165	• 5 59	907
150.00	944.50	353.00	• 458	1.497	•484	•771	•372	•640	•465	1.535	•478	333.	•374	.551
100.00	229.50	376.50	•31C	•975	•313	• 445	•326	•360	•316	• 989	•313	•519	•330	• 261
50.00	115.00	-23.50	• 269	•7 <u>8</u> 9	•270	•351	•096	• 363	•276	• 799	•272	• 426	•102	• 262
0.CO	0.00	0.00	•101	•554	•068	• 353	•061	-260	•106	•547	•069	•433	•070	.1FG

#### (B) RIGHT WING, INBUARD STATION

#### WING LCADINGS

SHEAR, LBS	MOMENT, IN-LBS	TORQUE, IN-LBS	MU 1	MU 2	MU 3	MU 4	MU 5	MII 6	MU 11	MU 12	M1 13	MU <b>.</b> 4	MU 15	MU 16
								., ,			.,, 15	1,0 1		,0 ,0
25.00		110.00	•017	•676	• 009	•675	•042	•691	•017	.681	009	•69U	.044	•682
50.00		9년 • <b>7</b> 5	• 066	1.344	•018	1.319	•047	1.293	•068	1.355	•020	1.349	•051	1.278
75.00		230.75	• (92	1.869	• 025	1.820	.108	1.833	•093	1.903	•027	1.856	•110	1.814
100.00		218.50	•154	2.488	•067	2.348	•119	2.324	•155	2.516	•068	2.394	•123	2.296
125.00		367.50	•184	2.933	• 082	2.724	•167	2.744	•184	2.966	•063	2.779	•189	2.711
150.00		355.00	• 259	3.474	•141	3.136	•205	3.127	• 256	3.516	•140	3.191	•207	3.087
. 200.00		685.00	•314	4.090	•164	3.636	•363	3.733	•311	4.147	•160	3.702	•361	3.688
	10293.25	660.50	• 460	4.854	• 319	4.211	• 406	4.240	•455	4.923	•309	4.261	• 403	4.186
	11006.25	1025.50	•515	5.360	•371	4 • 495	•599	4.605	•508	5.33€	•357	4.566	•588	4.553
-	11719.25	1001.50	• 669	5.766	• 534	4.808	•644	4.886	•659	5.833	•512	4.865	•633	4.822
	11829.75	1399.00	•700	5.929	•570	4.896	<ul><li>884</li></ul>	4.886	•691	6.025	•546	4.976	.871	4.818
	11936.75	1373.50	• t 74	6.162	• 769	4.890	•920	4.988	•964	6.261	.741	4.954	.905	4.913
	13629.25	1483.50	•924	6.963	•77€	5.573	•965	5.724	•911	7.083	.751	5.645	•951	5.636
	15178.25	1472.25	• 989	7.676	•812	6.230	•974	6.343	•974	7.800	•784	6.306	959	6.236
	16437.75	1604.25	1.027	8.256	•827	6.736	1.033	5.895	1.013	8.398	.801	6.823	1.018	6.781
	17692.50	1592.00	1.105	8•889	688.	7.283	1.048	7.407	1.088	9.025	.849	7.367	1.032	7.274
	18648.50	1741.60	1.136	9.337	• 897	7.663	1.120	7.836	1.121	9.495	.867	7.761	1.102	7.699
	19604.00	1728.50	1.214	5•∂37	• 959	6.073	1.135	8.222	1.199	9.992	•927	0.185	1.120	8.071
	20920.00	2058.50	1.280	10.497	1.005	8.596	1.303	8.837	1.260	10.660	.971	8.707	1.279	8.673
	22230.00	2034.00	1.430	11.219	1.147	9.183	1.347	9.353	1.412	11.390	1.105	9.306	1.323	9.176
	22943.00	2399.00	1.486	11.634	1.198	9.463	1.540	9.712	1.464	11.800	1.151	9.565	1.507	9.531
	23656.00	2375.00	1.643	12.129	1.362	9.793	1.589	10.007	1.621	12.300	1.366	9.928	1.556	9.811
	23766.50	2772.50	1.675	12.309	1.348	9.899	1.833	10.004	1.653	12.460	1.341	10.014	1.798	9.604
900.00	23973.50	2747.00	1.845	12.519	1.592	9.883	1.866	10.107	1.824	12.700	1.533	10.003	1.833	9.901
	25566.00	2857.00	1.68	13.279	1.596	10.583	1.917	10.808	1.863	13.440	1.539	10.707	1.880	10.581
	27115.00	2845.75	1.955	13.989	1.635	11.243	1.930	11.428	1.931	14.160	1.576	11.391	1.895	11.181
975.00	29374.50	2977.75	1.593	14.569	1.647	11.773	1.995	11.978	1.965	14.750	1.567	11.919	1.957	11.721
1000.00	29629.25	2965.50	2.064	15.169	1.695	12.333	2.011	12.488	2.037	15.340	1.635	12.469	1.975	12.201
1025.00	30585.25	3114.50	2.093	15.609	1.711	12.713	2.062	12.908	2.066	15.790	1.649	12.879	2.046	12.621
1050.00	31540.75	3102.00	2.168	16.099	1.766	13.153	2.102	13.298	2.140	16.260	1.705	13.319	2.066	12.991
	32856.75	3432.00	2.227	16.739	1.813	13.663	2.269	13.90P	2.137	16.920	1.746	13.539	2.227	13.581
1150.00	34166.75	3407.50	2.373	17.439	1.947	14.263	2.314	14.428	2 - 3 4 5	17.620	1.077	14.449	2.273	14.051
1200.00	34979.75	3772.50	2.428	17.529	2.001	14.543	2.510	14.788	2.397	18.030	1.925	14.739	2.462	14.441
1250.00	35592.75	3748.56	2.593	16.329	2.161	14.893	2.558	15.0°A	2.551	18.520	2.076	15.065	2.507	14.711
1300.00	35703.25	4146.00	2.616	16.499	2.201	14.973	2.799	15.078	2.583	18.700	2.114	15.159	2.750	14.701
1350.00	35810.25	4120.56	2.789	18.719	2.396	14.963	2.835	15.188	2.755	18.930	2.307	15.149	2.794	14.791
		•				_ ,	_ •		· • · · ·	7.4.50	5 1 201	7 7 8 T 4 A	40104	140147

#### TABLE VII. - CONTINUED

#### (B) CONCLUDED

#### WING LOADINGS

SHEAP,	M 3M EPT,	TOROUL												
LBS	IN-LBS	IN-LBS	MU 1	¥U 2	PU 3	MU 4	MU 5	MU 6	MU 11	MU 12	MU 13	Mit 17	MII 3.5	WII 54
			_	-		, ,		110	10 11	170 12	70 I3	MU 14	MU 15	MU 16
1325.00	34117.75	4010.50	2.731	16.129	2.466	14.343	2.817	14.588	2.750	18.330	2.316	16 500	2 7/2	1 / 101
1300.00	32568.75	4021.75	2.733	17.469	2.357	13.693	2.815	13.99F	2.702	17.660	2.269	14.509	2.763	14.191
1275.00	31309.25	3889.75	2.710	16.949	2.374	13.193	2.759	13.478	2.681	17.140	2.263	13.059	2.759	13.611
1250.00	30054.50	3902.00	2.658	16.399	2.337	12.673	2.752	12.998	2.628	16.580		13.349	2.705	13.091
1225.00	29098.50	3753.00	2.633	15.989	2.323	12.303	2.685	12.578	2.604	16.170	2.246	12.619	2.695	12.611
1200.00	28143.00	3765.50	2.573	1:.539	2.374	11.893	2.670	12.218	2.543	15.710	2.233 2.184	12.439	2.630	12.201
1150.00	26827.00	3435.50	2.521	14.949	2.334	11.393	2.509	11.619	2.493	15.710	-	12.019	2.614	11.841
1100.00	25517.00	3460.00	2.390	14.269	2.110	10.833	2.466	11.128	2.411	14.430	2.147 2.027	11.519	2.457	11.231
1050.00	24804.00	3095.00	2.343	13.901	2.062	10.563	2.474	10.778	2.316	14.060	1.984	13.944	2.417	10.751
1000.00	24091.00	3119.00	2.198	13.439	1.907	10.263	2.229	10.509	2.171	13.590		10.667	2.231	10.393
950.00	23980.50	2721.50	2.168	13.269	1.671	10.163	1.985	10.50P	2.142		1.635	10.354	2.198	10.131
900.00	23873.50	2747.00	2.000	13.059	1.67ե	10.173	1.949	10.415	1.973	13.420 13.210	1.803	10.274	1.945	10.131
875.00	22191.00	2637.CU	1.967	12.329	1.680	9.493	1.908	9.708	1.943		1.611	10.291	1.912	10.041
850.00	20632.00	2648.25	1.909	11.619	1.650	8.853	1.963	9.104	1.885	12.470	1.614	9.665	1.870	9.351
	19372.50	2516.25	1.675	11.049	1.639	8.353	1.646	3.166		11.760	1.502	8.953	1.864	8 • 751
800.00	18117.75	2528.50	1.510	10.439	1.596	7.823	1.833	8.068	1.853	11.190	1.572	8.447	1.807	8.216
	17161.75	2379.50	1.778	9.989	1.579	7.453	1.764		1.789	10.570	1.529	7.914	1.795	7.672
	16206.25	2392.00	1.710	9.501	1.523	7.047	1.748	7•639 7•265	1.758	10.210	1.513	7.533	1.726	7.307
700.00	14890.00	2062.00	1.651	F.661	1.477	6.543	1.562		1.691	9.623	1.459	7.124	1.710	6.943
650.00	13580.25	2086.f0	1.511	t.122	1.345	5.975	1.542	6•638 6•136	1.635	8.971	1.417	6.612	1.549	6.325
	12867.25	1721.50	1.459	7.733	1.295	5.705	1.344	5.764	1.496	8.222	1.289	6.039	1.509	5 • 833
550.00	12154.25	1745.50	1.309	7.232	1.135	5.369	1.298	5.490	1.445	7.625	1.244	5.765	1.319	5.460
500.00	12043.75	1348.CC	1.274	7.059	1.097	5.301	1.057	5.488	1.295	7.313	1.059	5.445	1.275	5.196
	11936.75	1373.50	1.099	6.019	507	5.306	1.037	5.400 5.380	1.263	7.140	1.056	5.364	1.035	5.197
425.00	10244.25	1263.50	. 061	6.059	896	4.627	•977	4.65₽	1.088	6.893	•860	5.376	1.001	5.099
400.00	8695.25	1274.75	994	5.320	• 860	3.976	• 969	4.035	1.053	6.118	• 557	4.667	•957	4 • 388
375.00	7435.75	1142.75	• <b>9</b> 5 7	4.735	• £49	3.470	•908		•986	5.365	•521	4.030	• 947	. 3 • 7€3
350.00	6161.00	1155.00	• £ 93	4.204	860	2.933	•900 •894	3.486	•950	4.771	•811	3.515	.888	3.246
325.00	5225.00	1006.00	• 6 46	3.639	• 782	2.546	•824	2.978	.97 <u>8</u>	4.128	•763	2.974	• 974	2.757
300.00	4269.50	1018.50	•771	3.132	•723	2.134		2.547	•P43	3.655	•746	2.563	• 8 0 5	2.336
250.00	2953.50	688.50	.702	2.456	•663	1.616	•805 •641	2.164	•759	3.140	•689	2.162	•787	1.969
200.00	1643.50	713.00	•551	1.701	•534		-	1.535	•703	2.449	•643	1.640	•628	1.349
150.00	930.50	348.60	490	1.273	• 480	1.034 .749	•597	1.018	•548	1.673	•50E	1.046	•586	• 85A
100.00	217.50	372.CC	•331	.763	• 420		• 404 357	•657	402	1.240	•460	.761	• 400	• 498
50.00	107.00	-25.50	• 292	•574	• 275	• 426	• 357	•375	•334	•720	•301	•432	•355	230
0.00.	0.00	0.00	119	•34E	• 275 • <b>C7</b> t	• 333	•116	• 373	•297	• 5 26	•266	• 345	•116	• 231
		·/ • ·	• * 1	● 21 <b>7</b> C	• ( / )	• 33F	•079	•269	•123	•267	<b>.</b> 070	.357	•052	•135

25.00

0.00

205.50

0.00

-12.50

0.00

TABL" VII.- CONCLUDED (C) PIGHT WING, MIDVING STATION

#### WING IDADINGS STRAIN-GAGE BRIDGE DUTPUTS, MILLIVOLTS SHEAR. MOMENT, TORQUE, LBS IN-LBS IN-LBS MU 7 Mt: 8 MU 9 MU 10 4U 17 MII JA MU 19 MU 20 25.00 942.50 110.00 .624 .704 .083 .672 .018 .703 .074 .642 50.00 1741.50 98.75 .10E 1.325 .113 1.225 .096 1.325 .099 1.173 75.00 2251.00 230.75 .147 1.696 .228 1.597 .131 1.691 ·206 1.525 100.00 2755.75 218.50 .255 2.096 .228 1.943 2.091 .233 .240 1.856 125.00 2961.75 367.50 .288 2.260 .267 2.071 .262 2.252 .390 1.976 150.00 3167.25 355.CO .436 2.153 .423 2.225 .402 2.398 .419 2.123 175.00 4109.75 465.00 .460 3.112 .519 2.854 .422 3.088 .479 2.720 200.00 4908.75 453.75 .546 3.727 .550 3.408 .50C 3.697 .502 3.255 225.00 5418.25 585.75 . 186 4.091 .664 3.779 •53£ 4.050 -510 3.610 250.00 5923.00 573.50 . €96 4.487 .703 4.124 .637 4.450 .644 3.937 275.00 6129.00 722.50 .729 4.549 .859 4.251 .666 4.506 .794 4.057 300.00 6334.50 710.00 . 877 4.799 .891 4.407 ·807 4.752 .822 4.203 325.CO 7277.00 820.00 .902 5.494 . 954 5.030 .828 5.434 .990 4.800 350.00 8076.00 808.75 .988 6.107 .965 5.583 .906 6.041 -904 5.330 375.00 8585.50 940.75 1.029 6.473 1.098 5.966 .942 6.403 1.011 5.692 400.00 9090.25 928.50 1.139 6.869 1.137 6.312 1.044 6.795 1.045 6.022 425.00 1077.50 9296.25 1.171 7.028 1.291 6.436 1.074 6.950 1.194 6.141 450.00 9501.75 1065.00 1.321 7.177 1.321 6.595 1.216 7.095 1.222 6.267 425.00 8559.25 955.00 1.293 6.493 1.220 5.873 1.193 6.397 1.133 5.592 400.00 7760.25 966.25 1.208 5.875 1.188 5.319 1.115 5.779 1.108 5.063 375.00 7250.75 F34.25 1.167 5.507 1.675 4.950 1.079 5.414 1.001 4.710 350.00 6746.00 P46.50 1.058 5.111 1.036 4.306 •977 5.071 .957 4.382 325.00 5540.00 697.50 1.025 4.948 . 882 4.480 4.860 .947 .818 4.260 6334.50 300.00 710.00 · £78 4.798 .849 4.325 4.714 .807 .789 4.116 275.00 5392.00 600.00 .852 4.541 •7€3 3.69P ·7e5 4.081 .730 3.510 250.00 4593.CO 611.25 .756 3.494 .753 3.145 .707 3.408 .706 2.982 225.00 4083.50 479.25 .725 3.114 .639 2.774 .671 3.042 .598 2.626 200.00 3575.75 491.50 .617 2.720 .599 2.429 •570 2.647 • 555 2.300 175.00 3372.75 342.50 · 584 2.556 . 445 2.302 .540 2.488 •416 2.160 150.00 3167.25 355.00 ·436 2.407 .414 2.147 2.341 .400 .397 2.033 125.00 2224.75 245.00 .412 1.708 .349 1.519 -360 1.653 .32R 1.430 100.00 1425.75 254.25 .327 1.093 •318 . 466 .301 1.041 .305 .961 75.00 916.25 124.25 .286 .724 .205 .593 .266 .677 .197 .547 50.00 411.50 136.50

.175

.145

-.002

.325

.160

.009

.166

.012

-.019

. 248

.119

-.036

.280

.121

-.025

.163

.014

-.013

.219

.095

-.046

.164

.135

-.005

# TABLE VIII. - LOADING FOR SIMULATED DESIGN CRUISE FLIGHT CONDITION

	APPLIEI (Each	) LOAD				LO	CATION							
	(Lucii	arrig)		LEFT WI	NG. INBOAF	RD		RIGHT WI	ING, INBOA	RD	RIG	нт мійс	, MIDWIN	G
				$Y_{W_1}$		X <sub>I-1</sub>		YW2		x <sub>W2</sub>		W <sub>3</sub>		
	N	(1bs)	) m	(in.)	m	(in)	m	2 (in.)	m	"2 (in.)	m	"3 (in)	.n	₩3 (in.)
1	111.21	25	1.723	67.83	0.110	4.35	1.720	67.70	0.112	4.40	0.958		0.112	4.40
2	111.21	25	1.578	62.13.	+0.011	-0.45	1.574	61.96	-0.011	-0.45	0.812	31.96	+0.011	-0.45
3	111.21	25	1.483	58.40	0.123	4.85	1.482	58.35	0.123	4.85	0.720	28.35	0.123	4.35
4	111.21	25	1.279	50.34	-0.012	-0.47	1.275	50.19	-012	-0.49	0.513	20.19	-0.012	-0.49
5	111.21	25	1.278	50.32	0.134	5.28	1.280	50.38	0.134	5.28	0.518	20.38	0.134	5.28
6	111.21	· 25	1.127	44.37	-0.012	-0.49	1.124	44.25	-0.012	-0.49	0.362	14.25	-0.012	-0.49
. 7	111.21	25	1.128	44.39	0.143	5.63	1.127	44.36	0.143	5.63	0.365	14.36	0.143	5.63
8	111.21	25	0.975	38.37	-0.013	-0.50	0.971	33.22	-0.013	-0.50	0.209	8.22	-0.013	-0.50
9	111.21	25	0.983	38.70	0.206	8.10	0.980	38.60	0.206	8.10	0.218	8.60	0.206	8.10
10	111.21	25	0.822	32.35	-0.013	-0.50	0.818	32.21	-0.013	-0.50	0.056	2.21	-0.013	-0.50
11	111.21	25	0.821	32.31	0.160	6.30	0.820	32.27	0.160	6.30	0.058	2.27	0.160	6.30
12	111.21	25	0.783	30.83	0.161	6.35	0.782	30.77	0.163	6.40	0.020	0.77	0.163	6.40
13	111.21	25	0.670	26.36	-0.012	-0.49	0.665	26.20	-0.012	-0.49				
14	111.21	25	0.678	26.69	0.243	9.55	0.673	26.50	0.241	9.48				
15	111.21	25	0.551	21.82	-0.013	-0.50	0.550	21.66	-0.013	-0.50				
16	111.21	25	0.554	21.80	0.174	6.87	0.553	21.77	0.173	6.83				
17	111.21	25	0.478	18.80	-0.011	-0.45	0.474	18.66	-0.013	-0.50				
18	111.21	25	0.440	17.33	0.182	7.15	0.439	17.29	0.182	7.15				
19	111.21	25	0.363	14.30	-0.012	-0.47	0.361	14.20	-0.013	-0.50				
20	111.21	25	0.362	14.26	0.185	7.30	0.362	14.26	0.185	7.30				
21	111.21	25	0.248	9.78	-0.011	-0.45	0.245	9.64	-0.013	-0.50				
22	111.21	25	0.249	9.80	0.191	7.52	0.247	9.71	0.192	7.54				
23	111.21	25	0.173	6.80	-0.011	-0.45	0.168	6.61	-0.012	-0.48				
24	111.21	25	0.134	5.26	0.198	7.80	0.133	5.24	0.197	7.77				
25	111.21	25	0.058	2.30	-0.012	-0.47	0.054	2.14	-0.013	-0.51				
26	111.21	25	0.058	2.29	0.203	8.00	0.056	2.21	0.202	7.95				
27	111.21	25	-0.017	-0.67	-0.011	-0.45	-0.021	-0.82	-0.012	-0.48				
28	111.21	25	-0.079	-3.12	0.232	9.14	-0.077	-3.03	0.234	9.20				
29	155.69	35	-0.093	-3.68	-0.011	-0.45	-0.099	-3.88	-0.012	-0.49				
30	66.72	15	-0.165	-6.50	0.236	9.30	-0.162	-6.39	0.239	9.40				
31	111.21	25	-0.209	-8.21	-0.011	-0.45	-0.213	-8.38	-0.013	-0.50				
32	111.21	25	-0.246	-9.70	0.242	9.51	-0.245	-9.64	0.243	9.58				

TABLE IX. - LOADING FOR SIMULATED DESIGN STRENGTH FLIGHT CONDITION (2.5 g MANEUVER).

	· APPL	IED LOAD					· L	OCATION						
		ch Wing)	LEF	T WING,	INBOARD	•	RIGHT	WING,I	NBOARD		RIG	HT WING	, MIDWIN	G
	;			Y <sub>W</sub> 1	X <sub>W 1</sub>		YW2		х	W <sub>2</sub>		$Y_{W_3}$	хн	3
	N	(1bs)	m	"1 (in.)	"] m	(in.)	2 m	(in.)	m	``2 (in.)	m	(in.)	m	(in.)
1	111.21	25	1.667	65.63	0.048	1.90	1.666	65.58	0.050	1.95	0.904	35.58	0.050	1.95
2	444.82	100	1.578	62.13	<b>-0.011</b>	-0.45	1.574	61.96	-0.011	-0.45	0.812	31.96	-0.011	-0.45
3	111.21	25	1.400	55.13	0.128	5.05	1.400	55.12	0.129	5.09	0.638	25.12	0.129	5.09
4	222.41	50	1.447	56.98	-0.010	-0.40	1.444	56.86	-0.011	-0.45	0.682	26.86	-0.011	-0.45
5	333.62	75	1.275	50.19	-0.012	-0.49	1.275	50.19	-0.012	-0.49	0.513	20.19	-0.012	-0.49
6	111.21	25	1.280	50.38	0.134	5.28	1.280	50.38	0.134	5.28	0.518	20.38	0.134	5.28
7	333.62	75	1.165	45.88	-0.012	~0.48	1.162	45.74	-0.012	-0.48	0.400	15.74	-0.012	-0.48
3	111.21	25	1.128	44.39	0.143	5.63	1.127	44.36	0.143	5.63	0.365	14.36	0.143	5.63
9	222.41	50	1.050	41.35	-0.013	-0.50	1.047	41.21	-0.013	-0.50	0.285	11.21	-0.013	-0.50
10	222.41	50	1.011	39.80	0.148	5.83	1.009	39.73	0.149	5.88	0.247	9.73	0.149	5.88
11	444.82	100	0.860	33.85	-0.013	-0.50	0.857	33.74	-0.013	-0.52	0.095	3.74	-0.013	-0.52
12	222.41	50	0.857	33.73	0.158	6.23	0.857	33.75	0.158	6.23	0.095	3.75	0.158	6.23
13	333.62	75	0.707	27.83	-0.013	-0.50	0.704	27.70	-0.013	-0.50				
14	333.62	75	0.705	27.75	0.166	6.53	0.707	27.82	0.166	6.53				
15	333.62	75	0.592	23.30	-0.013	-0.50	0.589	23.18	-0.013	-0.50				
16	222.41	50	0.554	21.80	0.174	6.87	0.554	21.80	0.171	6.75				
17	333.62	75	0.439	17.30	-0.012	-0.48	0.435	17.12	-0.012	-0.48				
18	333.62	75	0.401	15.77	0.182	7.15	0.401	15.78	0.183	7.20				
19	333.62	75	0.325	12.80	-0.012	-0.47	0.320	12.60	-0.012	-0.49				
20	222.41	50	0.286	11.27	0.189	7.45	0.284	11.19	0.190	7.48				
21	333.62	<b>7</b> 5	0.211	8.30	-0.011	-0.45	0.207	8.13	-0.013	-0.50				
22	222.41	50	0.172	6.77	0.196	7.70	0.171	6.72	0.197	7.74				
23	333.62	75	0.058	2.30	-0.012	-0.47	0.054	2.14	-0.013	~0.51				
24	222.41	50	0.058	2.29	0.203	8.00	0.056	2.21	0.202	7.95				
25	333.62	75	-0.055	-2.17	-0.011	-0.45	-0.060	-2.35	-0.013	-0.50				
26	222.41	50	-0.049	-1.92	0.230	9.05	-0.048	-1.89	0.232	9.13				
27	333.62	75	-0.169	-6.67	-0.011	-0.45	-0.174	-6.85	-0.013	-0.50				
28	222.41	50	-0.165	-6.50	0.236	9.30	-0.168	-6.60	0.236	9.30				
29	111.21	25	-0.209	,-8.21	-0.011	-0.45	-0.213	-8.38	-0.013	-0.50				
30	111.21	25	-0.246	-9.70	0.242	9.51	-0.249	-9.80	0.240	9.45				

TABLE X.- DESIGN CRUISE AND MANEUVER FLIGHT CONDITION WING LOADINGS AND ASSOCIATED STRAIN GAGE BRIDGE OUTPUTS

Design Flight Condition	Shear N (1bs.)	Wing loadings  Bending  Moment  N-m (inlb.) N-m	Torsional Moment (inlb.)		\$	Strain-q	gage brid	dge out <sub>l</sub>	outs, mil	llivolts	s, for -				
		Left wing, inboard		$^{\mu}$ 21	<sup>μ</sup> 22	<sup>μ</sup> 23	<sup>μ</sup> 24	<sup>μ</sup> 25	<sup>μ</sup> 26	<sup>μ</sup> 31	<sup>μ</sup> 32	<sup>μ</sup> 33	<sup>μ</sup> 34	<sup>μ</sup> 35	<sup>μ</sup> 36
Cruise	650	18698	2234	1.217	9.356	1.129	7.648	1.405	7.639	1.242	9.666	1.089	8.013	1.377	8.117
Maneuver	1450	43042	3148	3.134	22.135	2.972	17.932	2.472		3.234	22.895	2.906	16.798	2.424	18.344
		Right wing, inboard		$^{\mu}$ 1	$^{\mu}$ 2	$^{\mu}$ 3	<sup>μ</sup> 4	$^{\mu}$ 5	<sup>μ</sup> 6	<sup>μ</sup> 11	<sup>μ</sup> 12	<sup>μ</sup> 13	<sup>μ</sup> 14	<sup>μ</sup> 15	<sup>μ</sup> 16
Cruise	650	18634	2251	1.424	9.404	1.037	7.455	1.416	7.803	1.412	9.559	0.976	7.570	1.375	7.678
Maneuver	1450	42910	3139	3.595	21.840	2.724	17.673	2.483			•		17.867		
		Right wing, midwing		<sup>μ</sup> 7	<sup>μ</sup> 8	<sup>μ</sup> 9	<sup>μ</sup> 10	<sup>μ</sup> 17	<sup>μ</sup> 18	<sup>μ</sup> 19	<sup>μ</sup> 20				2, 120,
Cruise	300	4732	963	0.810	3.607	1.082	3.049	0.763	3.542	1.106	2.897				
Maneuver	650	11228	837	2.398	8.402	1.645	7.633	2.237	8.291	1.491	7.222				

# TABLE XI.- SUMMARY OF SELECTED STRAIN-GAGE BRIDGES, LOAD COEFFICIENTS, PROBABLE ERRORS, AND ACCURACY EVALUATION

#### A. Left Wing, Inboard Station.

Load Selected Load coefficient measurement bridges ± probable error	calibration loading	of load correlation estimate coefficient
V, N 23 762.0 ± 37.8 N/mV (171.3 ± 8.5 lb/mV)	2022 11	6 N .99985
(1b) 35 $693.0 \pm 41.4 \text{ N/mV}$ ( $155.8 \pm 9.3 \text{ lb/mV}$ )	(567 lbs) (±1	2.5 lbs)
36 132.1 $\pm$ 4.0 N/mV (29.7 $\pm$ 0.9 1b/mV)		
M, N-m 23 -121.1 ± 9.8 N-m/mV (-1071.6 ± 87.0 in1b/r		8 N-m .99992
(in1b) 36 279.5 $\pm$ 1.7 N-m/mV ( 2473.6 $\pm$ 14.7 in1b/r	mV) (15084 in1bs) (±2	44.6 in1bs)
T, N-m 23 - $79.5 \pm 4.3 \text{ N-m/mV}$ (-703.4 ± 38.3 in1b/r		N-m .99967
(in1b) 35 220.1 $\pm$ 4.7 N-m/mV (1947.8 $\pm$ 41.8 in1b/r	mV) (1737 in1bs) (±5	6.6 inlbs)
36 4.1 $\pm$ 0.4 N-m/mV ( 36.7 $\pm$ 3.9 in1b/m	mV)	

# TABLE XI.- CONTINUED

### B. Right Wing, Inboard Station.

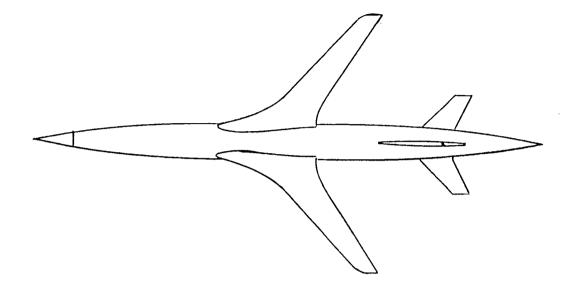
Load measurement	Selected bridges	Load coefficient ± probable error	Average wing calibration loading	Probable error of load estimate	Multiple correlation coefficient
V, N	13	800.2 ± 33.8 N/mV ( 179.9 ± 7.6 lb/m		±62 N-m	.99976
(16)	4	$141.9 \pm 4.0 \text{ N/mV}$ ( $31.9 \pm 0.9 \text{ lb/m}$	V) (477 lbs)	(±13.9 lbs)	
	15	$708.6 \pm 31.6 \text{ N/mV}$ ( $159.3 \pm 7.1 \text{ lb/m}$	<b>V</b> )		
M, N-m (inlb)	13	-129.1 ± 11.7 N-m/mV (-1142.3 ± 103.9 in.		±32 N-m	.99986
	4	288.7 ± 1.8 N-m/mV ( 2555.2 ± 16.3 in.	-1b/mV) (12700 in1bs)	(±287.1 in1bs)	
T, N-m (inlb)	13	- 86.9 ± 3.8 N-m/mV (-769.3 ± 33.6 in.	-1b/mV) 165 N-m	±7 N-m	.99903
	4	$4.4 \pm 0.5 \text{ N-m/mV}$ ( $39.3 \pm 4.0 \text{ in.}$	-lb/mV) (1458.7 inlbs)	(±61.7 inlbs)	
	15	214.6 ± 3.6 N-m/mV ( 1894.6 ± 31.6 in.	-1b/m/V)		

## C. Right Wing, Midwing Station.

Load measurement	Selected bridges		efficient ble error	Average wing calibration loading	Probable error of load estimate	Multiple correlation coefficient
V, N (1b)	7 18	593.8 ± 15.6 N/mV 79.2 ± 3.6 N/mV	( 133.5 ± 3.5 lb/mV) ( 17.8 ± 0.8 lb/mV)	792 N (178.1 1bs)	±24 N (±54 lbs)	.99971
	9	512.4 ± 15.6 N/mV	( 115.2 ± 3.5 lb/mV)			
M, N-m (in1b)	18	46.9 ± 12.5 N-m/mV	( 415.5 ± 110.5 in1b/mV)	409 N-m	±14 N-m	.99964
	9	$29.7 \pm 9.7 \text{ N-m/mV}$	( 263.2 ± 85.6 in1b/mV)	(3616.9 inlbs)	(120.0 111105)	
	10	$107.7 \pm 12.7 \text{ N-m/mV}$	( 952.9 ± 112.6 in1b/mV)			
T, N-m (in1b)	7	-41.2 ± 3.1 N-m/mV	(-364.8 ± 27.1 in1b/mV)	48 N-m	±5 N-m (±40.1 in1bs)	.99754
	18	$-25.2 \pm 4.0 \text{ N-m/mV}$	$(-223.3 \pm 35.5 \text{ inlb/mV})$	(423.4 in1bs)	(±40.1 111103)	
	9	$123.9 \pm 3.2 \text{ N-m/mV}$	$(1096.5 \pm 28.4 in1b/mV)$			
	10	29.3 4.2 N-m/mV	$(259.1 \pm 36.9 \text{ inlb/mV})$			

TABLE XII.- EVALUATION OF PREDICTED LOADS FOR TWO SIMULATED FLIGHT LOADINGS

	Design cruise simulated wing loading						Design maneuver simulated wing loading						
	Shear		Bending moment		Torque		Shear		Bending moment		Torque		
	N	(1bs.)	N-m	(in. lbs.)	N-m	(in. lbs.)	N	(1bs.)	N-m	(in.lbs.)	N-m	(in. lbs.)	
	Left wing, inboard station						Left wing, inboard station						
Calculated	2886.9	(649)	2132	(18868)	247	(2186)	6369.9	(1432)	4767	(42195)	373	(3304)	
Actual	2891.3	(650)	2113	(18698)	264	(2334)	6449.9	(1450)	4863	(43042)	356	(3148)	
Difference	-4.4	(-1)	19	(170)	-17	(-148)	-80.1	(-18)	<b>-</b> 96	(-847)	18	(156)	
% - Error	-0.2	-0.2	0.9	0.9	-6.3	-6.3	-1.2	-1.2	-2.0	-2.0	5.0	5.0	
	Right wing, inboard station						Right wing, inboard station						
Calculated	2811.3	(632)	2018	(17864)	243	(2147)	6294.2	(1415)	4750	(42046)	365	(3228)	
Actual	2891.3	(650)	2105	(18634)	254	(2251)	6449.9	(1450)	4848	(42910)	355	(3139)	
Difference	-80.1	(~18)	<b>-</b> 87	(-770)	-11	(-104)	-155.7	(-35)	<del>-</del> 98	(-864)	10	(89)	
% - Error	-2.8	-2.8	4.1	4.1	-4.6	-4.6	-2.4	-2.4	-2.0	-2.0	2.8	2.8	
	Right wing, midwing station					Right wing, midwing station							
Calculated	1316.7	(296)	527	(4662)	101	(890)	2926.9	(658)	1260	(11151)	119.22	(1055)	
Actual	1334.5	(300)	535	(4732)	108	(963)	2891.3	(650)	1269	(11228)	94.56	(837)	
Difference	-17.8	(-4)	-8	(-70)	-7	(-73)	35.6	(8)	<b>-</b> 9	(-77)	94.36 25	(218)	
% - Error	-1.3	-1.3	-1.5	-1.5	<b>-7.</b> 6	-7.6	1.2	1.2	-0.7	-0.7	26.0	26.0	



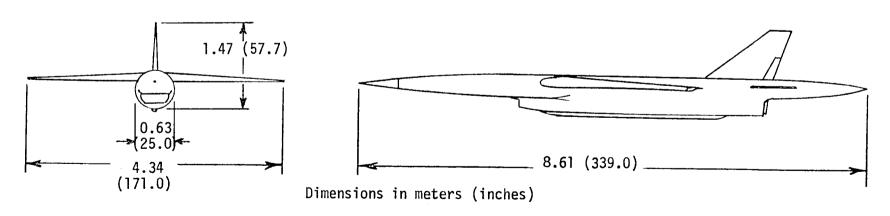


Figure 1.- General arrangement of BQM-34F drone aircraft with ARW-1 wing.

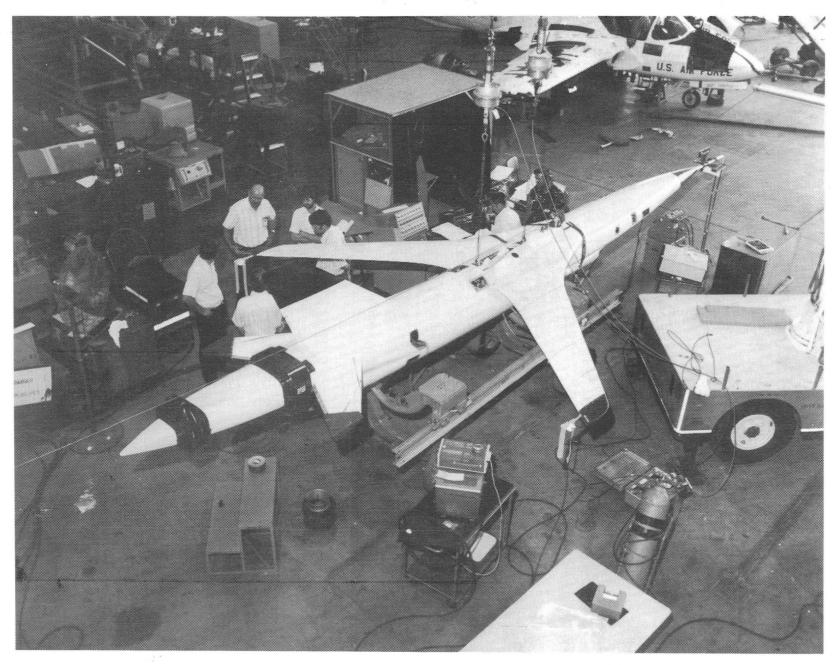


Figure 2.- Photograph of the aircraft and wing during assembly checkout.

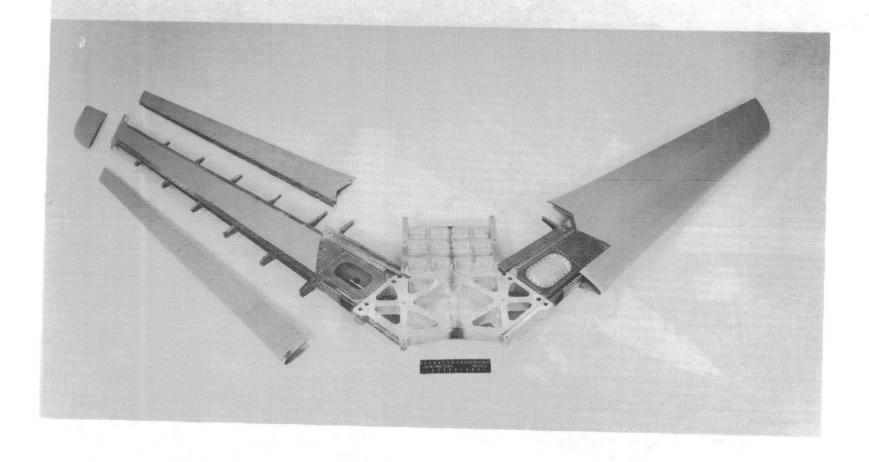


Figure 3.- Photograph of wing.

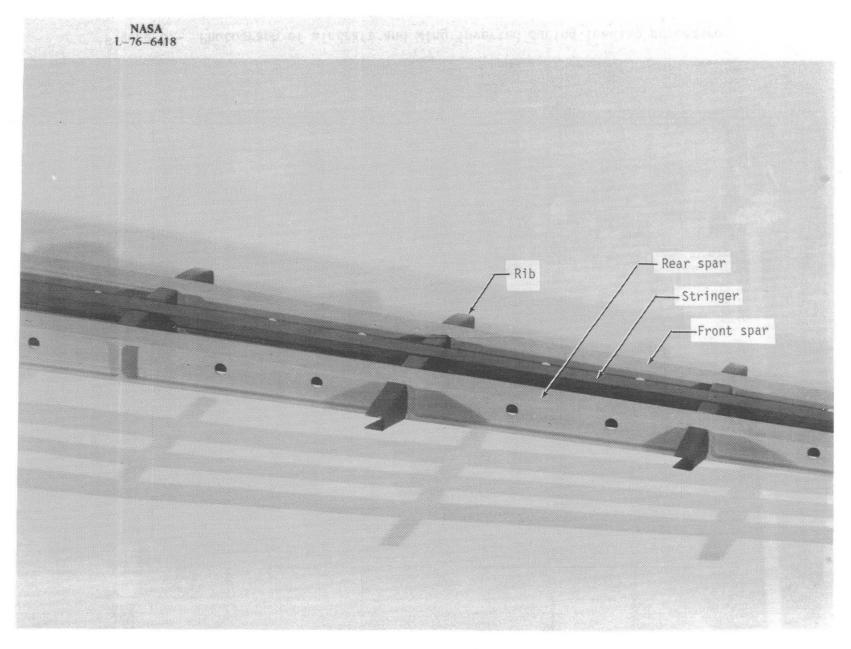


Figure 4.- Photograph of primary wing structure.

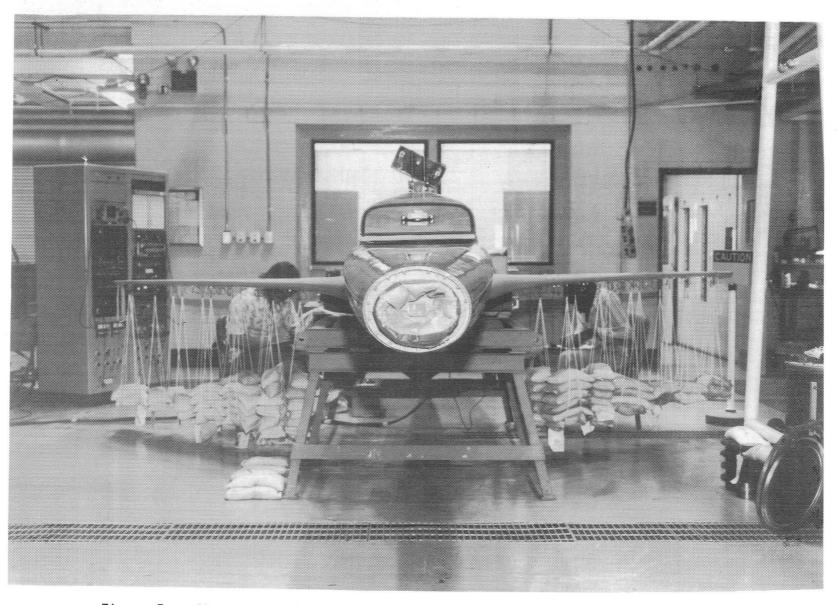


Figure 5.- Photograph of aircraft and wing inverted during loading procedure.

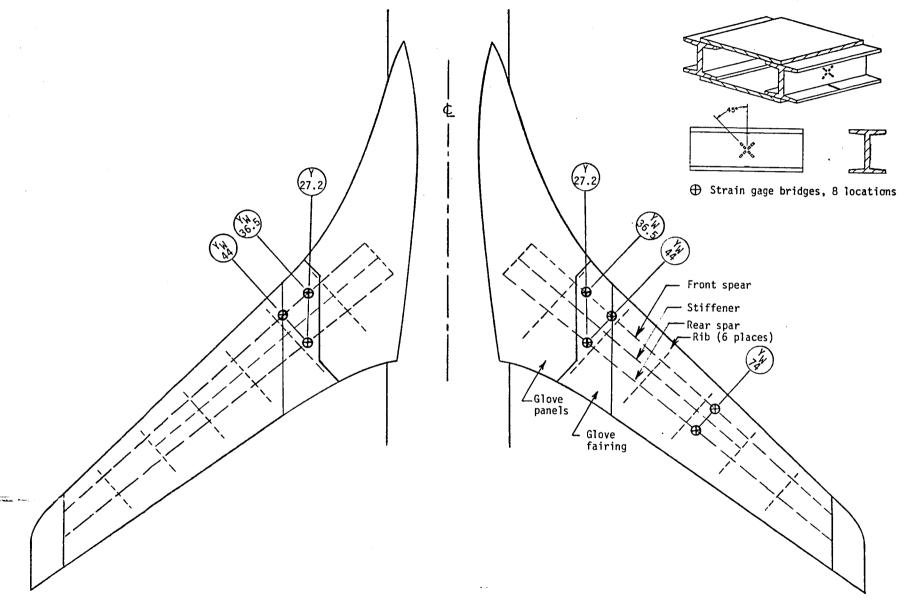
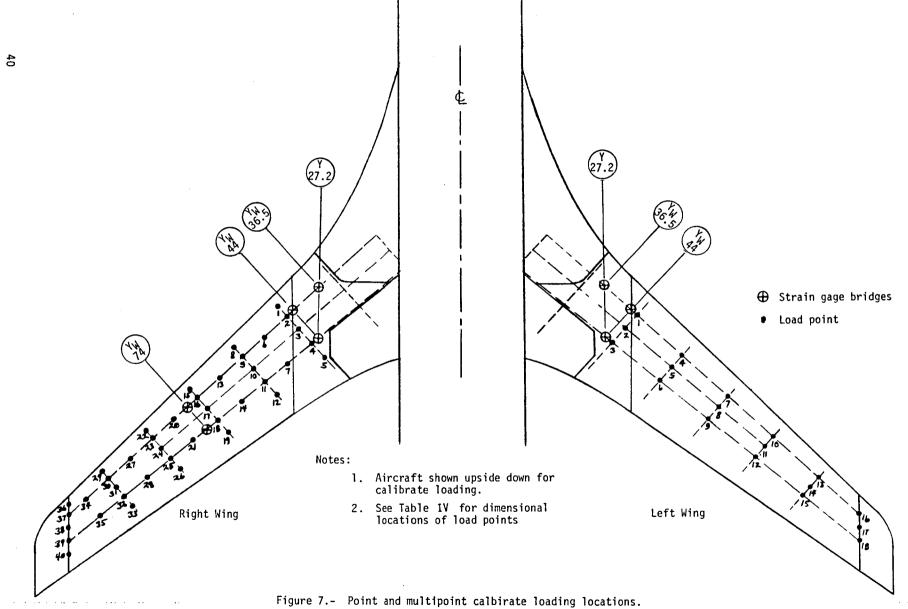


Figure 6.- Strain gage bridge locations.



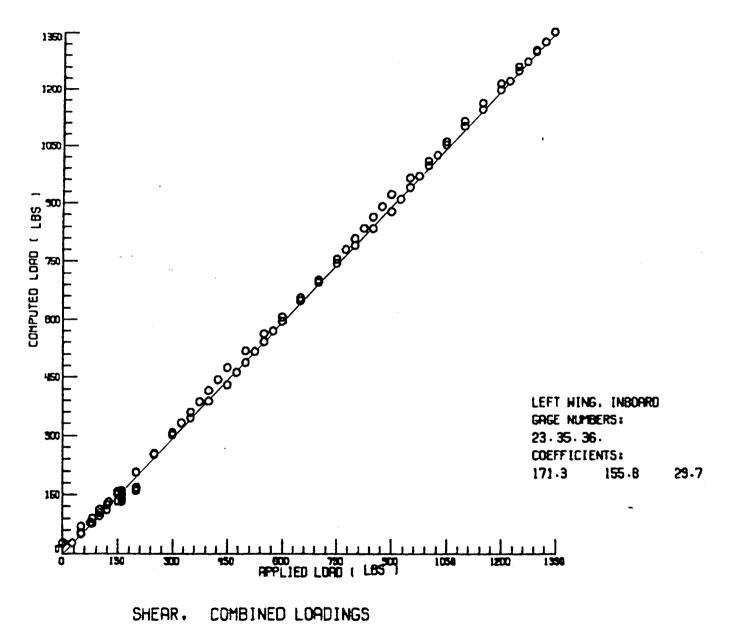


Figure 8.- Correlation of computed shear loads with applied calibration shear loads for the left wing inboard station.

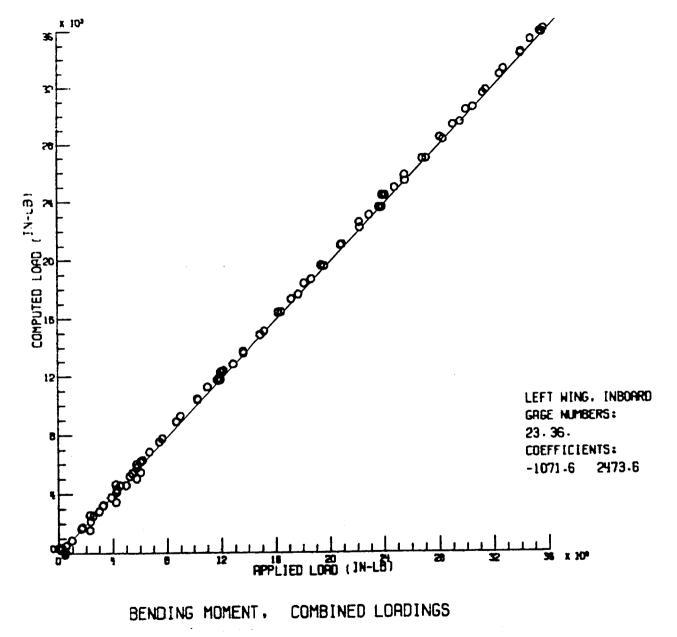


Figure 9.- Correlation of computed bending moment loads with applied calibration bending moment loads for the left wing inboard station.

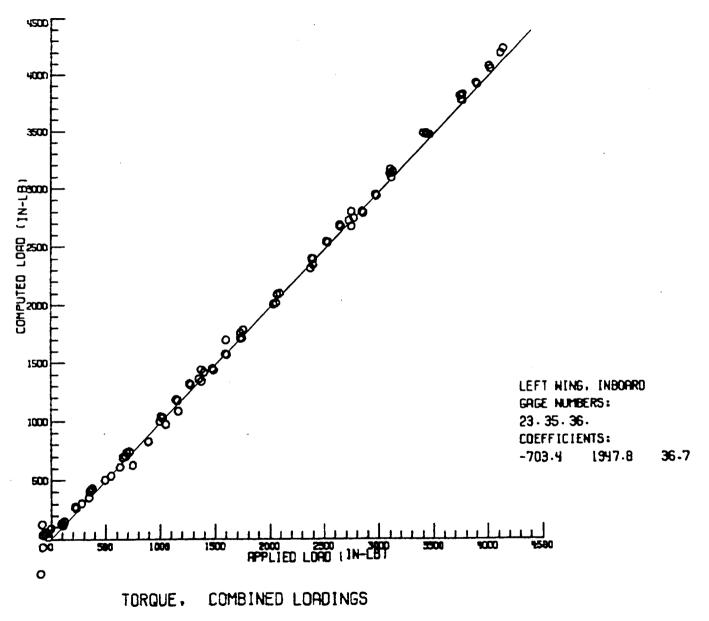


Figure 10.- Correlation of computed torque loads with applied calibration torque loads for the left wing inboard station.

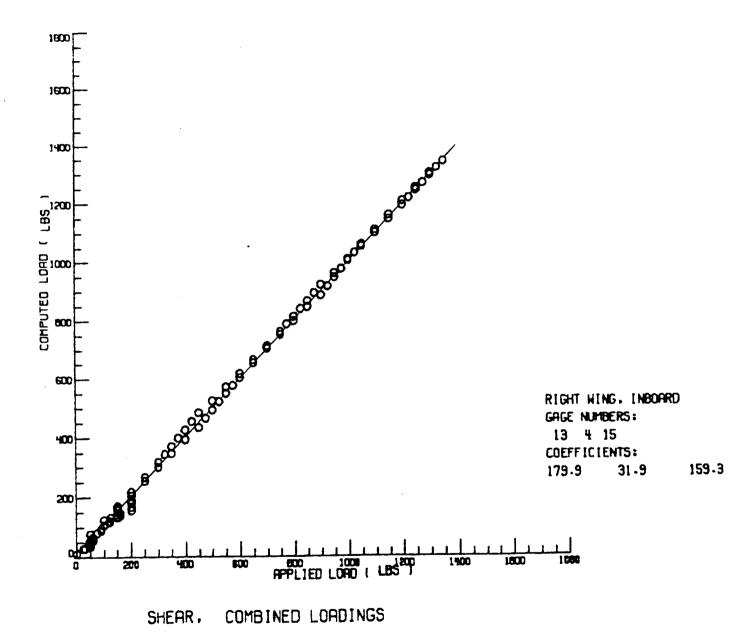


Figure 11.- Correlation of computed shear loads with applied calibration shear loads for the right wing inboard station.

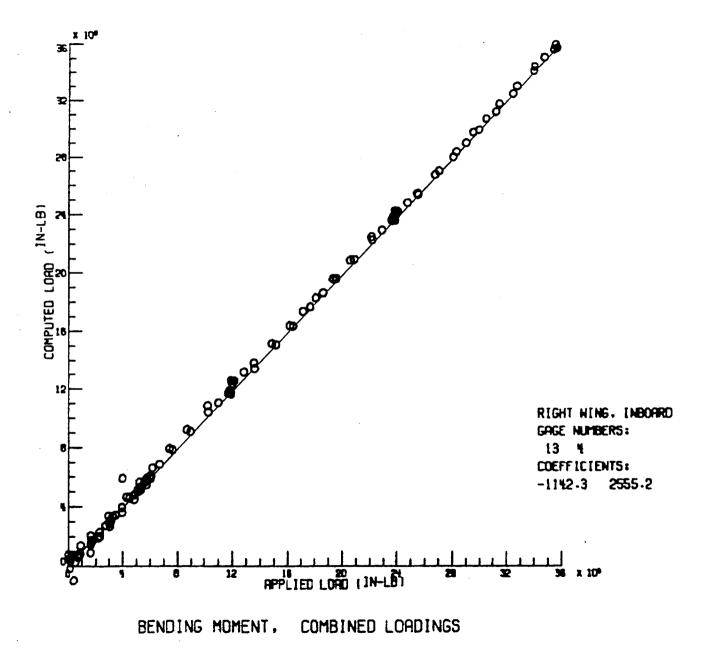


Figure 12.- Correlation of computed bending moment loads with applied calibration bending moment loads for the right wing inboard station.

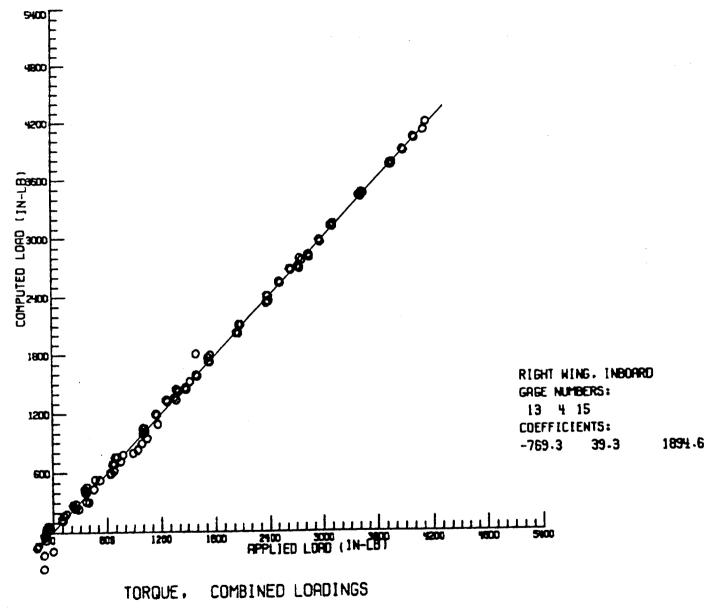


Figure 13.- Correlation of computed torque loads with applied calibration torque loads for the right wing inboard station.

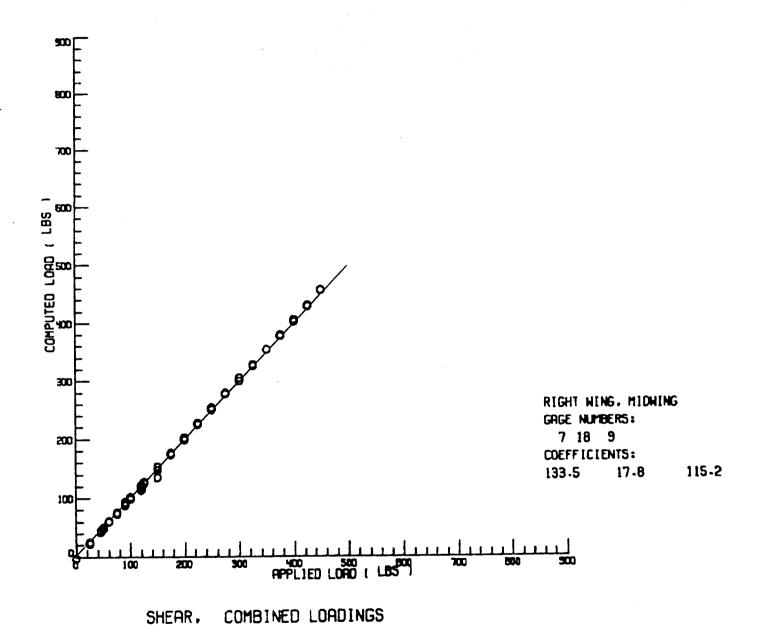


Figure 14.- Correlation of computed shear loads with applied shear loads for the right wing midwing station.

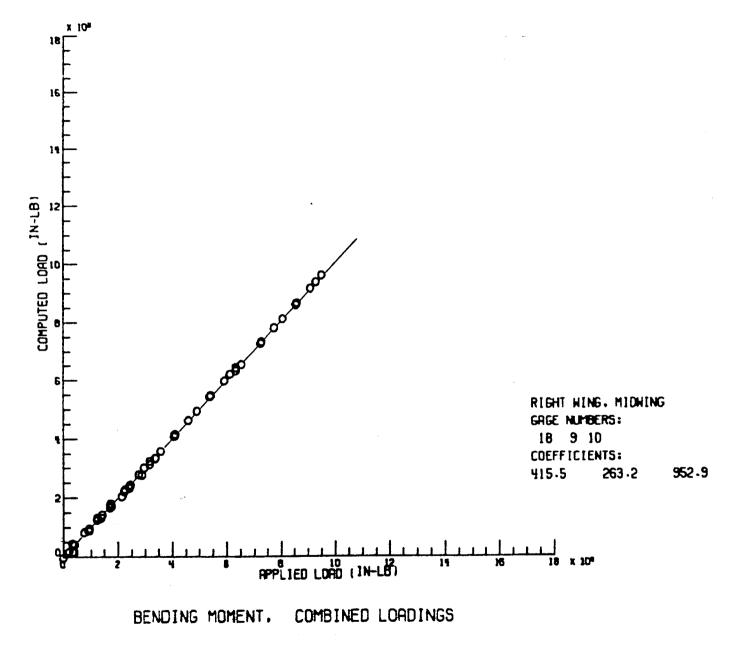


Figure 15.- Correlation of computed bending moment loads with applied bending moment load for the right wing midwing station.

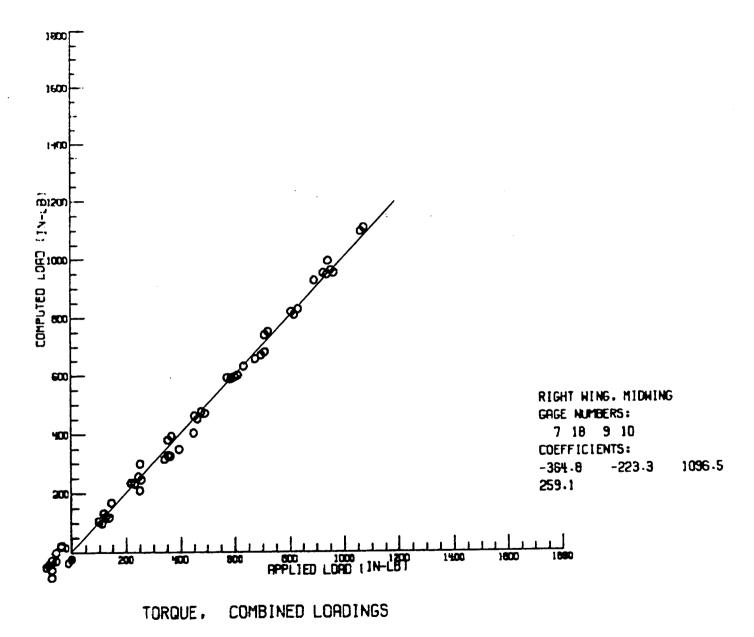


Figure 16.- Correlation of computed torque load with applied torque load for the right wing midwing station.

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